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(54) **PRESSURE TESTING VALVE AND METHOD OF USING THE SAME**

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This patent is subject to a terminal disclaimer.

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E21B 34/10	(2006.01)
E21B 49/00	(2006.01)
E21B 34/08	(2006.01)

(52) **U.S. Cl.**

CPC ***E21B 34/14*** (2013.01); ***E21B 34/08*** (2013.01); ***E21B 34/102*** (2013.01); ***E21B 49/008*** (2013.01)

(58) **Field of Classification Search**

USPC 166/374, 332.1

See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

4,627,492	A *	12/1986	MacLaughlin	.... 166/250.08
5,404,956	A	4/1995	Bohlen et al.	
6,491,116	B2	12/2002	Berscheidt et al.	
6,695,050	B2	2/2004	Winslow et al.	
6,695,051	B2	2/2004	Smith et al.	
6,976,534	B2	12/2005	Sutton et al.	
7,195,067	B2	3/2007	Manke et al.	

(Continued)

FOREIGN PATENT DOCUMENTS

WO	2009029437 A1	3/2009
WO	2012164236 A1	12/2012

OTHER PUBLICATIONS

Filing receipt and specification for patent application entitled "Pressure Testing Valve and Method of Using the Same," by Donald Smith, et al., filed Aug. 30, 2012 as U.S. Appl. No. 13/599,044.

(Continued)

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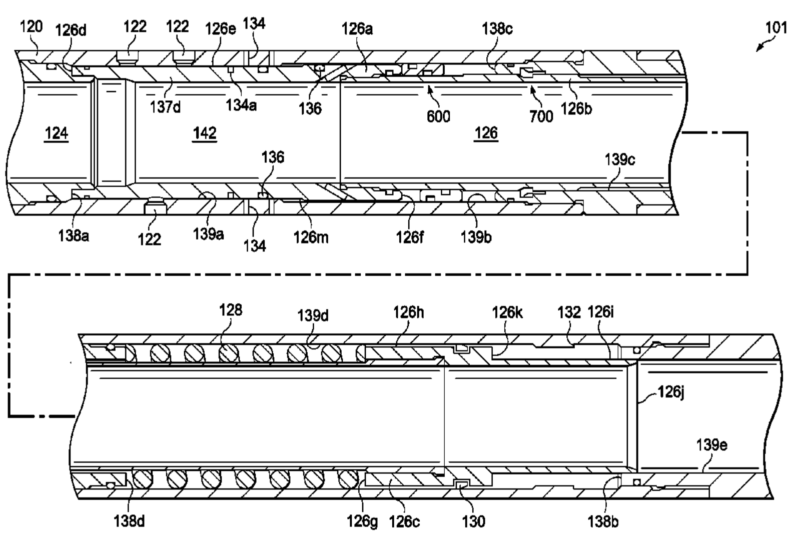
(57) **ABSTRACT**

A wellbore servicing system and method are disclosed. The wellbore servicing system includes a casing string and a pressure testing valve. The pressure testing valve includes a housing, a sliding sleeve, and a deactivatable locking assembly. The housing includes ports and an axial flowbore. The sliding sleeve is positioned within the housing and is transitional between first, second, and third positions. When the sliding sleeve is in the first and second positions, the sliding sleeve blocks fluid communication via the ports. When the sliding sleeve is in the third position, it does not block such fluid communication. Application of a fluid pressure transitions the sliding sleeve from the first to the second position, and a reduction in fluid pressure transitions the sliding sleeve from the second to the third position. When activated, the locking assembly inhibits movement of the sliding sleeve toward the third position.

19 Claims, 9 Drawing Sheets



(56) **References Cited**

U.S. PATENT DOCUMENTS

7,337,852	B2	3/2008	Manke et al.
7,373,973	B2	5/2008	Smith et al.
7,510,017	B2	3/2009	Howell et al.
7,559,363	B2	7/2009	Howell et al.
7,617,871	B2	11/2009	Surjaatmadja et al.
7,673,673	B2	3/2010	Surjaatmadja et al.
7,878,255	B2	2/2011	Howell et al.
7,946,340	B2	5/2011	Surjaatmadja et al.
7,963,331	B2	6/2011	Surjaatmadja et al.
8,146,673	B2	4/2012	Howell et al.
8,215,404	B2	7/2012	Makowiecki et al.
2005/0199399	A1	9/2005	Hayter et al.
2008/0135248	A1	6/2008	Talley et al.
2009/0308588	A1	12/2009	Howell et al.
2011/0042107	A1 *	2/2011	Chambers et al. 166/386
2011/0253383	A1	10/2011	Porter et al.
2012/0205120	A1	8/2012	Howell
2012/0205121	A1	8/2012	Porter et al.

OTHER PUBLICATIONS

Filing receipt and specification for patent application entitled "Pressure Testing Valve and Method of Using the Same," by Matthew Todd Howell, et al., filed Jan. 22, 2013 as U.S. Appl. No. 13/746,957.
International Search Report and Written Opinion issued in PCT/US2014/012115, mailed Nov. 18, 2014 (12 pages).
International Preliminary Report on Patentability issued in related PCT Application No. PCT/US2014/012115, mailed Aug. 6, 2015 (9 pages).

* cited by examiner

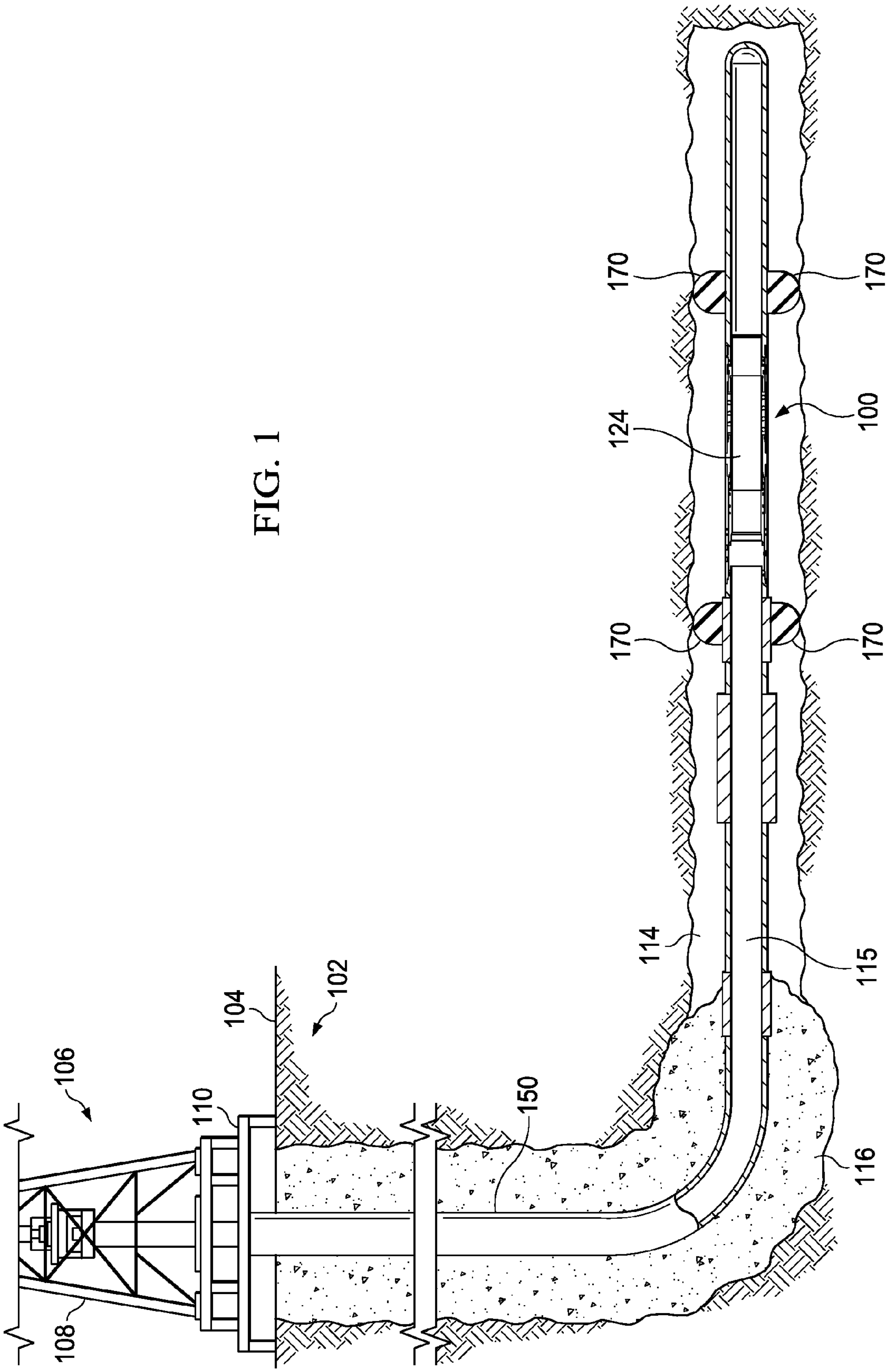
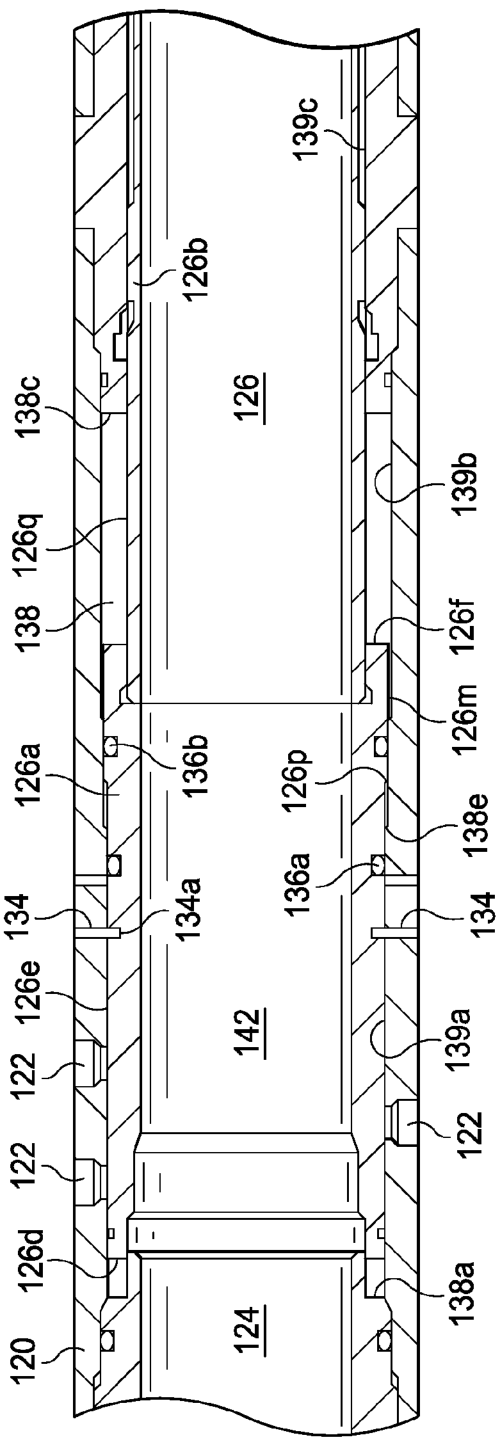


FIG. 1

FIG. 2



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126b
126
138c
139b
126q
138
126f
126m
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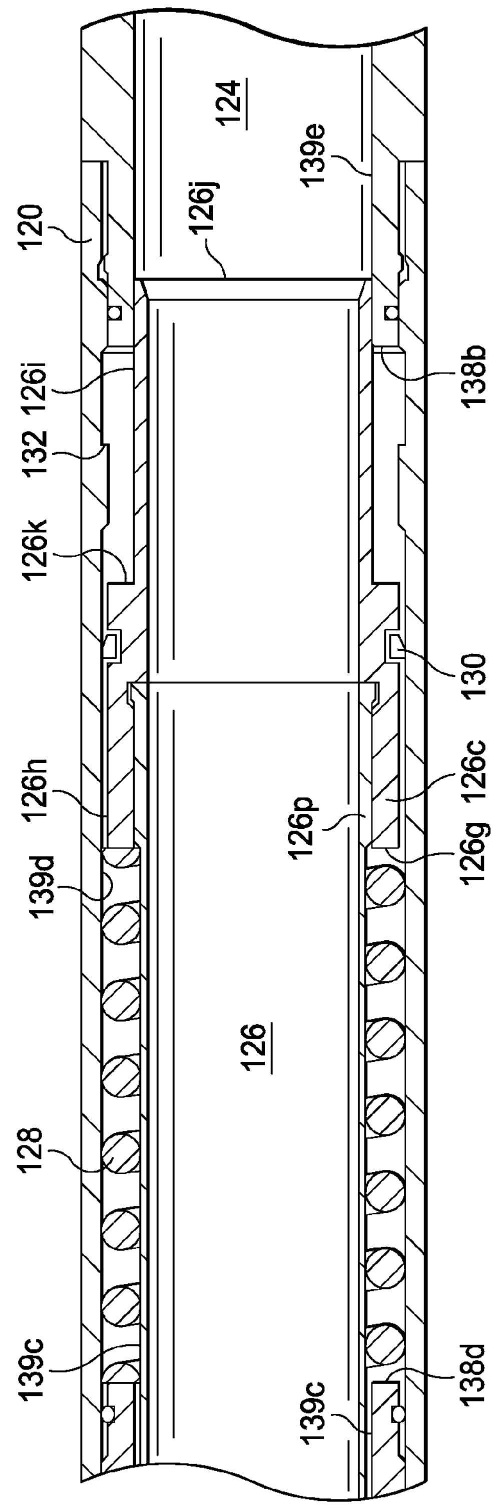
122
126d
124
138a
120



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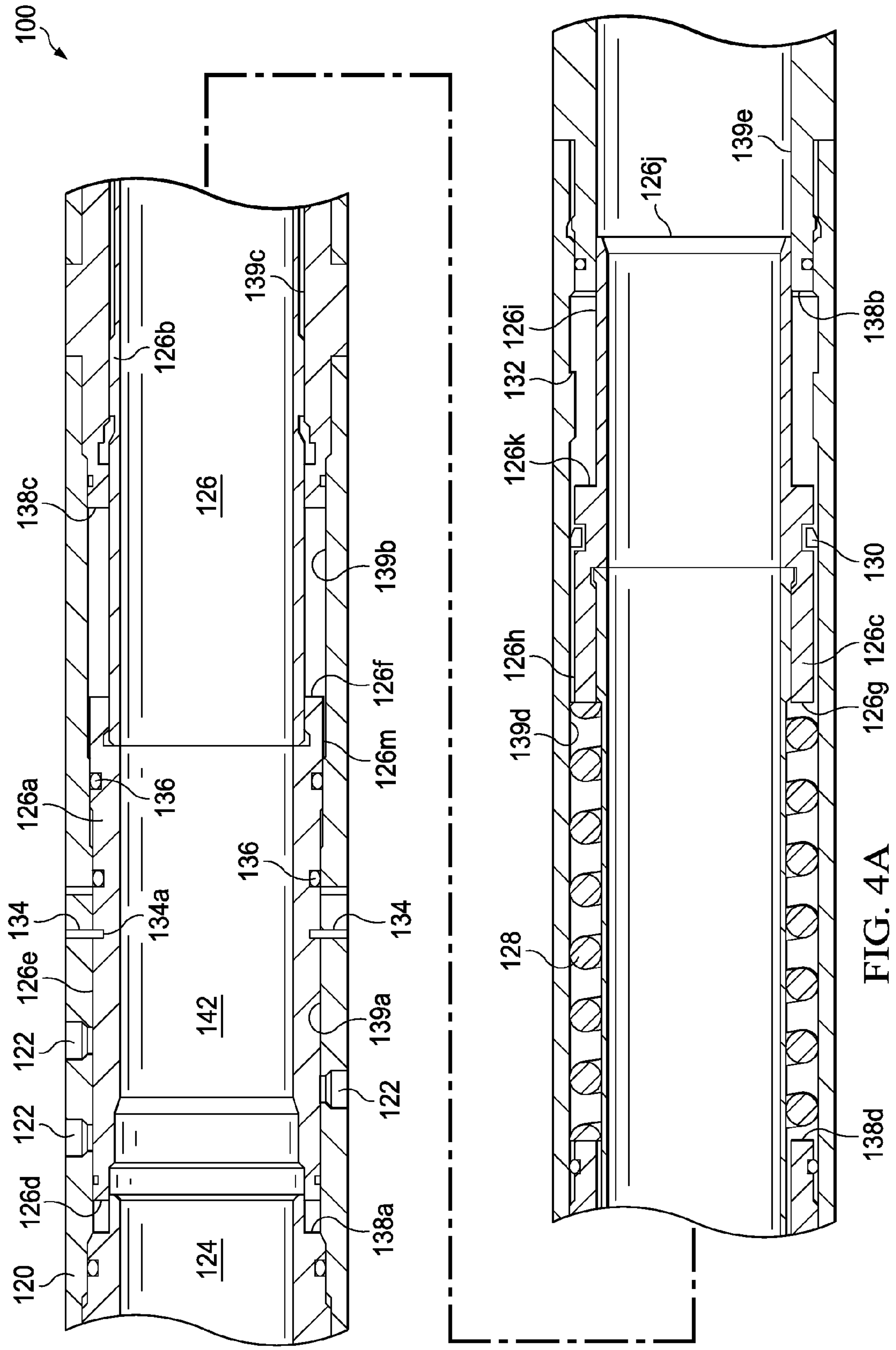
138d

FIG. 3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126d
138a
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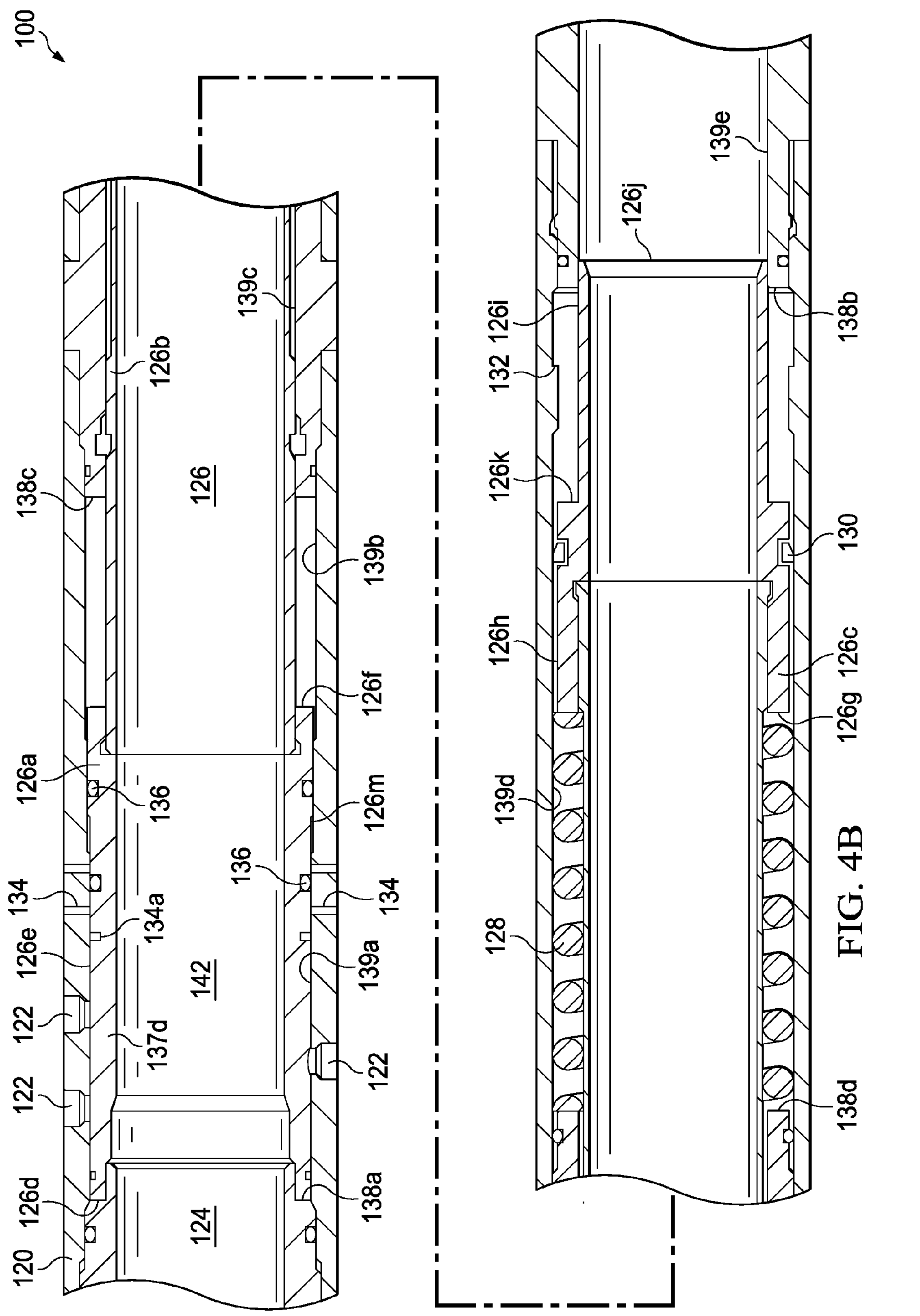
128
138d

FIG. 4A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139a
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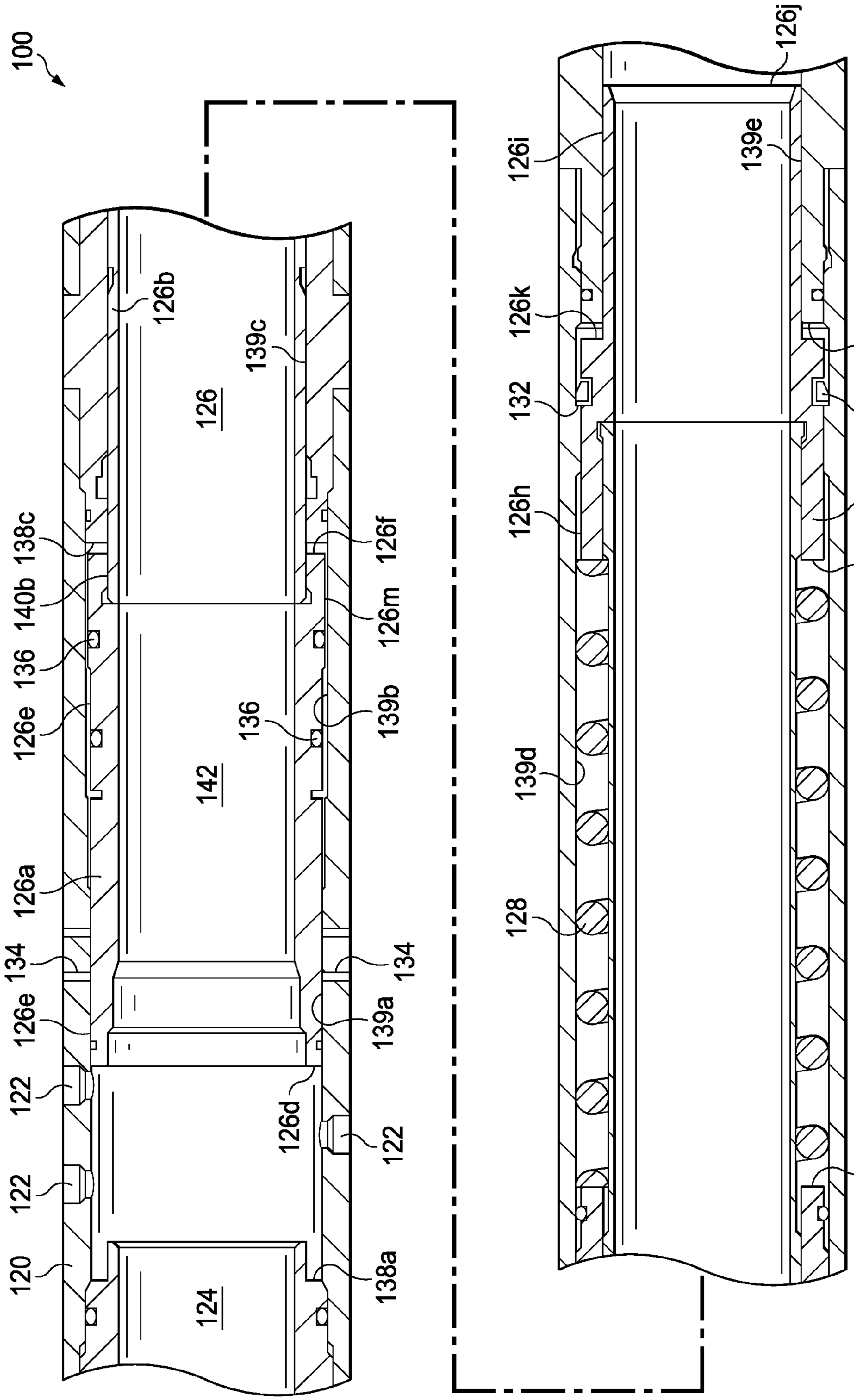
126g
138d

FIG. 4B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126d
122
122
120
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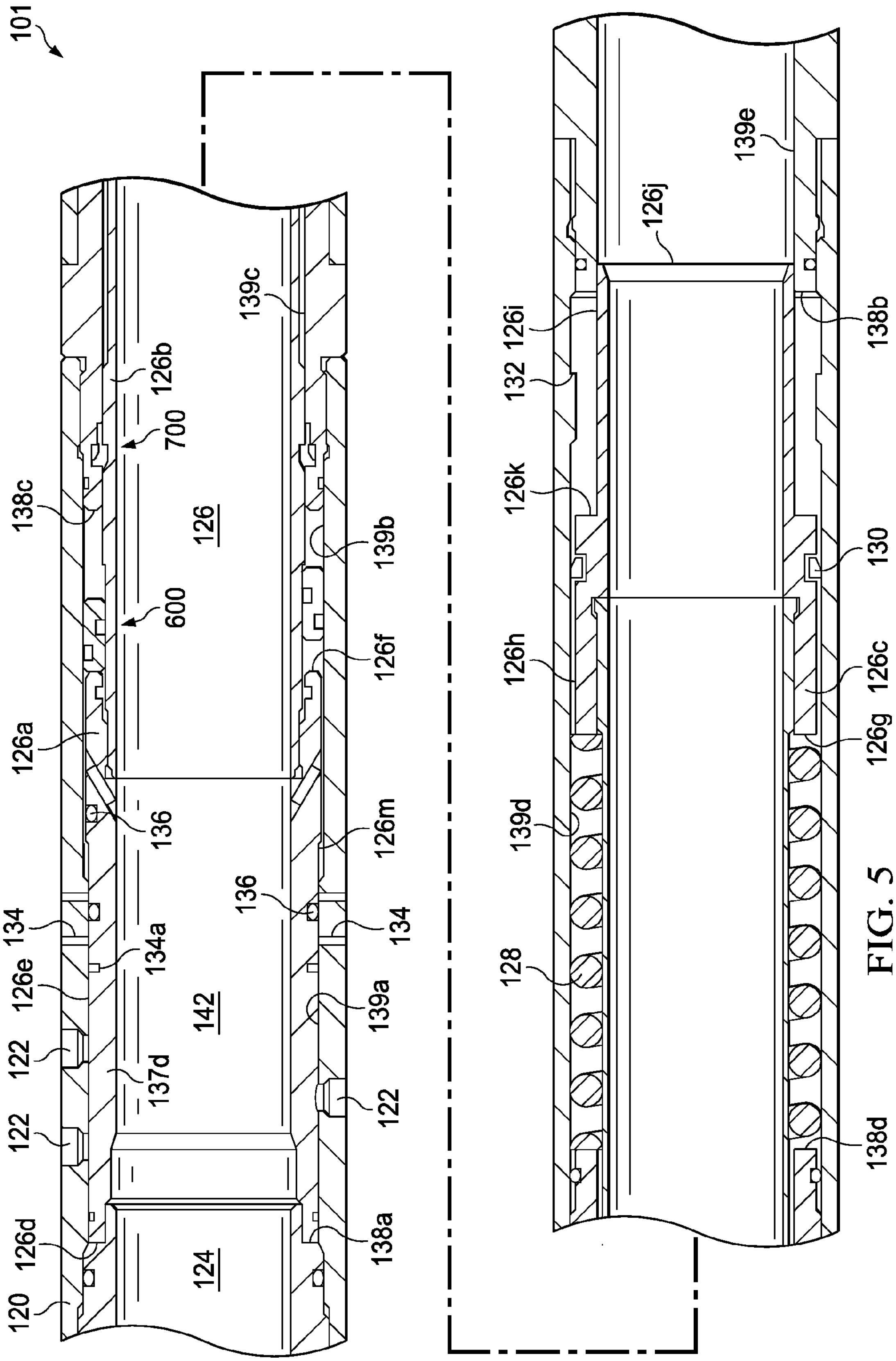
128
138d

FIG. 4C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122
126d
124
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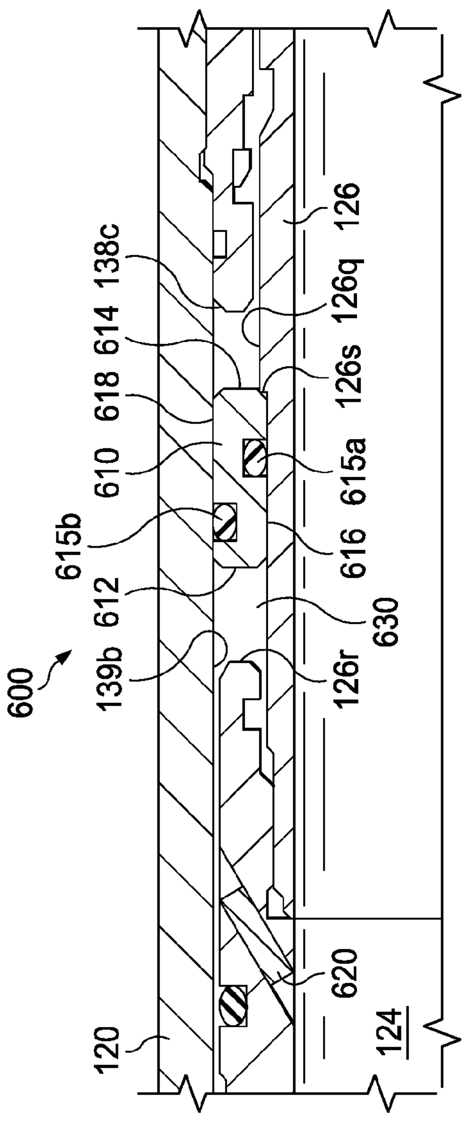
126g
139d
128
138d

FIG. 5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126s
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126r
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120

FIG. 6A

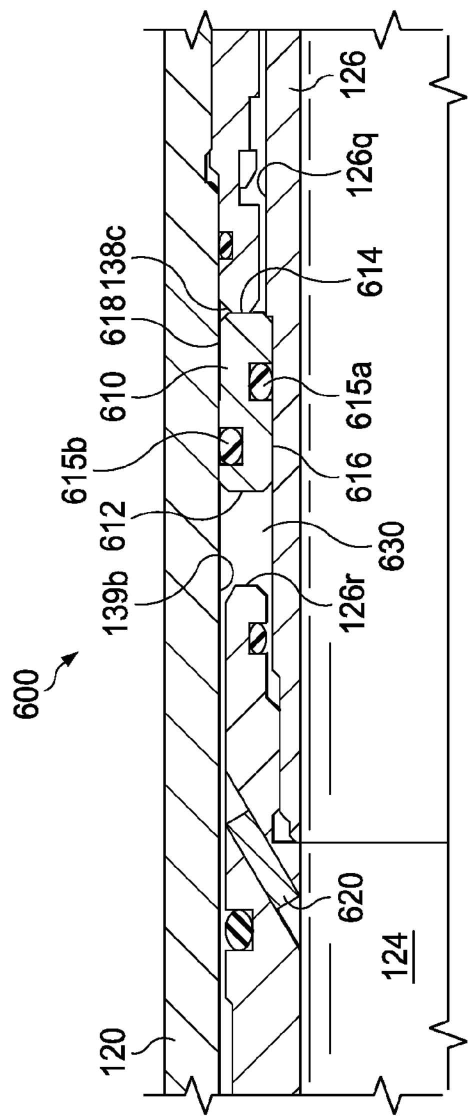
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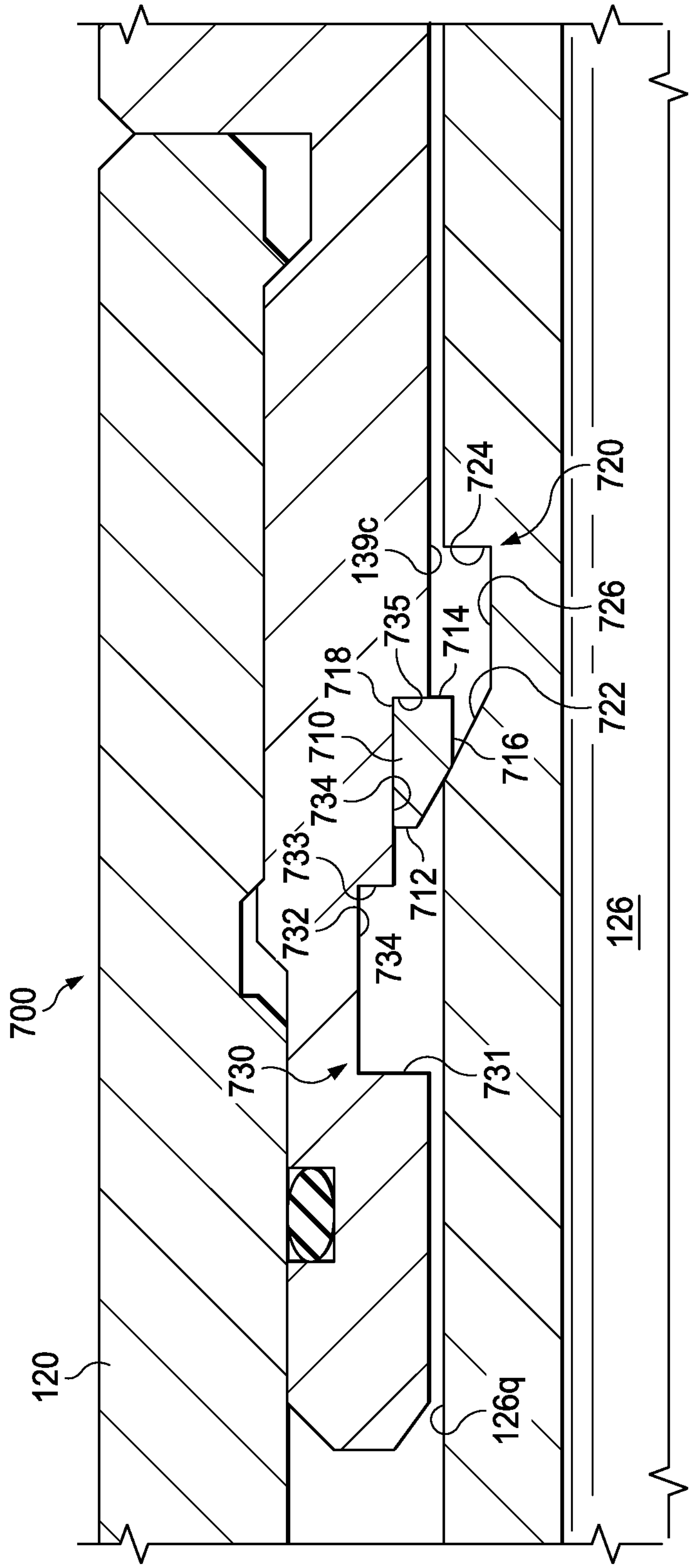
FIG. 6B



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733
712
732
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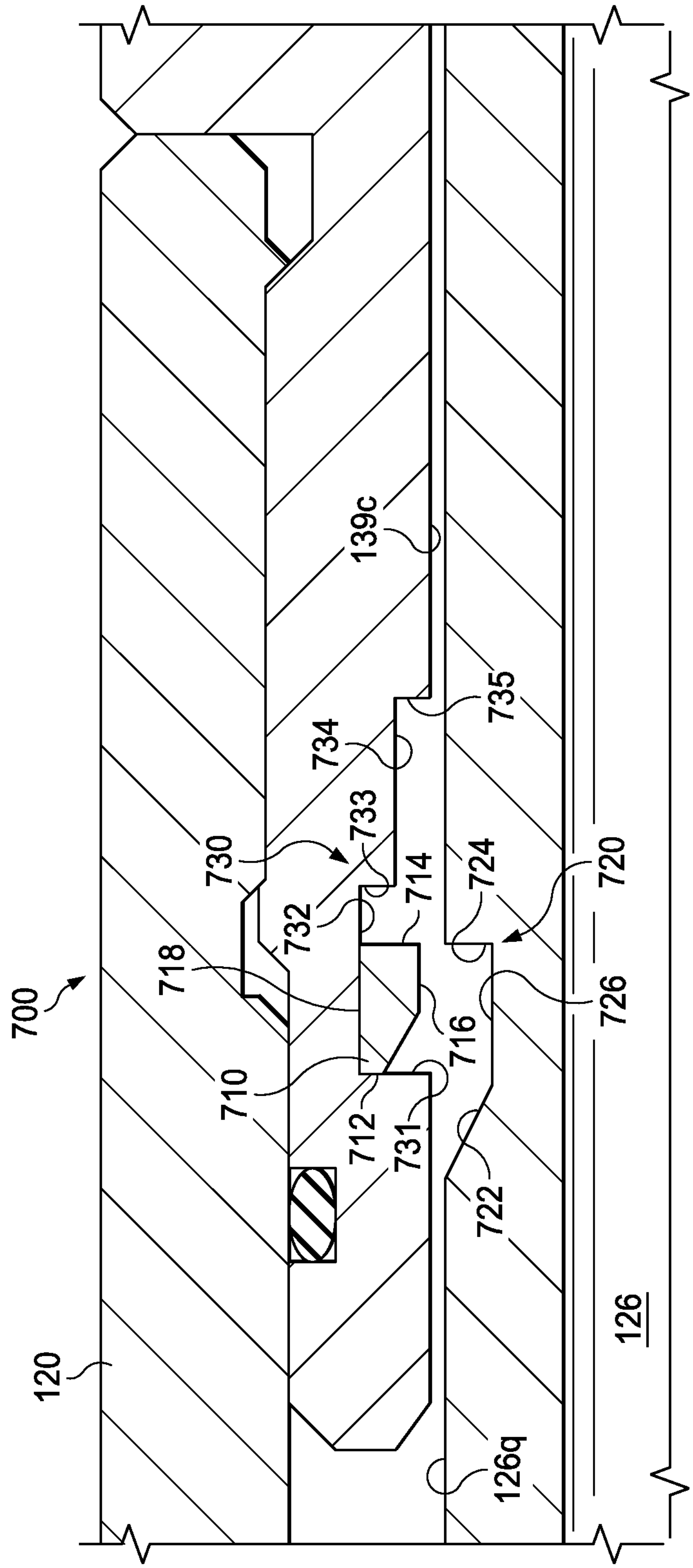
700
730
731
126
120
126q

FIG. 7A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120
139c
735
734
733
730
732
714
724
720
718
710
712
731
716
726
722
126
126q

FIG. 7B

PRESSURE TESTING VALVE AND METHOD OF USING THE SAME

CROSS-REFERENCE TO RELATED APPLICATIONS

Not applicable.

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

Not applicable.

REFERENCE TO A MICROFICHE APPENDIX

Not applicable.

BACKGROUND

Hydrocarbon-producing wells often are stimulated by hydraulic fracturing operations, wherein a servicing fluid such as a fracturing fluid or a perforating fluid may be introduced into a portion of a subterranean formation penetrated by a wellbore at a hydraulic pressure sufficient to create or enhance at least one fracture therein. Such a subterranean formation stimulation treatment may increase hydrocarbon production from the well.

When wellbores are prepared for oil and gas production, it is common to cement a casing string within the wellbore. Often, it may be desirable to cement the casing within the wellbore in multiple, separate stages. Furthermore, stimulation equipment may be incorporated within the casing string for use in the overall production process. The casing and stimulation equipment may be run into the wellbore to a predetermined depth. Various “zones” in the subterranean formation may be isolated via the operation of one or more packers, which may also help to secure the casing string and stimulation equipment in place, and/or via cement.

Following placement of the casing string and stimulation equipment within the wellbore, it may be desirable to “pressure test” the casing string and stimulation equipment, to ensure the integrity of both, for example, to ensure that a hole or leak has not developed during placement of the casing string and stimulation equipment. Pressure-testing generally involves pumping a fluid into an axial flowbore of the casing string such that a pressure is internally applied to the casing string and the stimulation equipment and maintaining that hydraulic pressure for sufficient period of time to ensure the integrity of both, for example, to ensure that a hole or leak has not developed. To accomplish this, no fluid pathway out of the casing string can be open, for example, all ports or windows of the fracturing equipment, as well as any additional routes of fluid communication, must be closed or restricted.

Following the pressure test, it may be desirable to provide at least one route of fluid communication out of the casing string. Conventionally, the methods and/or tools employed to provide fluid pathways out of the casing string after the performance of a pressure test are configured to open upon exceeding the pressure levels achieved during pressure testing, thereby limiting the pressures that may be achieved during that pressure test. Such excessive pressure levels required to open the casing string may jeopardize the structural integrity of the casing string and/or stimulation equipment, for example, by requiring that the casing and/or various other wellbore servicing equipment components be subjected to pressures near or in excess of the pressures for which such casing string and/or wellbore servicing component may be

rated. Thus, a need exists for improved pressure testing valves and methods of using the same.

SUMMARY

Disclosed herein is a wellbore servicing system comprising a casing string, and a pressure testing valve, the pressure testing valve incorporated within the casing string and comprising a housing comprising one or more ports and an axial flowbore, and a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing and transitional from a first position to a second position, and from the second position to a third position, wherein, when the sliding sleeve is in the first position and the second position, the sliding sleeves blocks a route of fluid communication via the one or more ports and, when the sliding sleeve is in the third position the sliding sleeve does not block the route of fluid communication via the one or more ports, wherein the pressure testing valve is configured such that application of a fluid pressure of at least an upper threshold to the axial flowbore causes the sliding sleeve to transition from the first position to the second position, and wherein the pressure testing valve is configured such that a reduction of the fluid pressure to not more than a lower threshold applied to the axial flowbore causes the sliding sleeve to transition from the second position to the third position, and a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured such that, when activated, the deactivatable locking assembly will inhibit movement of the sliding sleeve in the direction of the third position, and when deactivated, the deactivatable locking assembly will not inhibit movement of the sliding sleeve in the direction of the third position.

Also disclosed herein is a wellbore servicing method comprising positioning casing string having a pressure testing valve incorporated therein within a wellbore penetrating the subterranean formation, wherein the pressure testing valve comprises a housing comprising one or more ports and an axial flowbore, a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing, wherein the sliding sleeve is configured to block a route of fluid communication via one or more ports when the casing string is positioned within the wellbore, and a floating piston assembly slidably disposed between the housing and the sliding sleeve, wherein the floating piston assembly is configured so as to not apply longitudinal force to the sliding sleeve, applying a fluid pressure of at least an upper threshold to the axial flowbore, wherein, upon application of the fluid pressure of at least the upper threshold, the sliding sleeve continues to block the route of fluid communication and the floating piston assembly continues to not apply a longitudinal force to the sliding sleeve, and reducing the fluid pressure to not more than a lower threshold, wherein, upon reduction of the fluid pressure to not more than the lower threshold, the sliding sleeve allows fluid communication via one or more ports of the housing and the floating piston assembly applies a downward force to the sliding sleeve.

Further disclosed herein is a wellbore servicing tool comprising a housing comprising an axial flowbore, and a sliding sleeve, wherein the sliding sleeve is slidably, longitudinally movable within the housing; and a floating piston assembly slidably disposed between the housing and the sliding sleeve, wherein the floating piston is configured such that, when unactivated, the floating piston assembly will not apply a force to the sliding sleeve in either a first longitudinal direction or a second longitudinal direction, and when activated,

the floating piston assembly will apply a force to the sliding sleeve in the first longitudinal direction.

Further disclosed herein is a wellbore servicing system comprising a casing string, and a pressure testing valve, the pressure testing valve incorporated within the casing string and comprising a housing comprising one or more ports and an axial flowbore, and a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing and transitional from a first position to a second position, and from the second position to a third position, wherein, when the sliding sleeve is in the first position and the second position, the sliding sleeves blocks a route of fluid communication via the one or more ports and, when the sliding sleeve is in the third position the sliding sleeve does not block the route of fluid communication via the one or more ports, wherein the pressure testing valve is configured such that application of a fluid pressure of at least an upper threshold to the axial flowbore causes the sliding sleeve to transition from the first position to the second position, and wherein the pressure testing valve is configured such that a reduction of the fluid pressure to not more than a lower threshold applied to the axial flowbore causes the sliding sleeve to transition from the second position to the third position, and a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured such that, when activated, the deactivatable locking assembly will inhibit movement of the sliding sleeve in the direction of the third position, and when deactivated, the deactivatable locking assembly will not inhibit movement of the sliding sleeve in the direction of the third position.

Further disclosed herein is a wellbore servicing method comprising positioning casing string having a pressure testing valve incorporated therein within a wellbore penetrating the subterranean formation, wherein the pressure testing valve comprises a housing comprising one or more ports and an axial flowbore, a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing in a first position in which the sliding sleeve is configured to block a route of fluid communication via one or more ports when the casing string is positioned within the wellbore, and a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured so as to inhibit movement of the sliding sleeve in the direction of a third position, applying a fluid pressure of at least an upper threshold to the axial flowbore, wherein, upon application of the fluid pressure of at least the upper threshold, the sliding sleeve transitions to a second position in which the sliding sleeve continues to block the route of fluid communication, and wherein, upon movement of the sliding sleeve from the first position in the direction of the second position, the deactivatable locking assembly is configured so as to not inhibit movement of the sliding sleeve in the direction of a third position; and reducing the fluid pressure to not more than a lower threshold, wherein, upon reduction of the fluid pressure to not more than the lower threshold, the sliding sleeve transitions to a third position in which the sliding sleeve allows fluid communication via one or more ports of the housing.

Further disclosed herein is a wellbore servicing tool comprising a housing comprising an axial flowbore, and a sliding sleeve, wherein the sliding sleeve is slidably, longitudinally movable within the housing, and a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured such that, when activated, the deactivatable locking assembly will inhibit movement of the sliding sleeve in a first longitudinal direction and will not inhibit movement in a second longitudinal direction, wherein the first direction is generally opposite of the second direction, and when deactivated, the deactivatable locking assembly will not inhibit movement of the sliding sleeve the first direction.

BRIEF DESCRIPTION OF THE DRAWINGS

For a more complete understanding of the present disclosure and the advantages thereof, reference is now made to the following brief description, taken in connection with the accompanying drawings and detailed description:

FIG. **1** is a partial cut-away view of an operating environment of a pressure testing valve depicting a wellbore penetrating a subterranean formation and a casing string having a pressure testing valve incorporated therein and positioned within the wellbore;

FIG. **2** is a cut-away view of an upper portion of a pressure testing valve;

FIG. **3** is a cut-away view of a lower portion of a pressure testing valve;

FIG. **4**A is a partial cut-away view of an embodiment of a pressure testing valve in a first configuration;

FIG. **4**B is a partial cut-away view of an embodiment of a pressure testing valve in a second configuration;

FIG. **4**C is a partial cut-away view of an embodiment of a pressure testing valve in a third configuration;

FIG. **5** is a partial cut-away view of an embodiment of a pressure testing valve comprising a floating piston assembly and a deactivatable locking assembly;

FIG. **6**A is a partial cut-away view of an embodiment of a floating piston assembly;

FIG. **6**B is a partial cut-away view of an embodiment of a floating piston assembly;

FIG. **7**A is a partial cut-away view of an embodiment of a deactivatable locking assembly in a first configuration; and

FIG. **7**B is partial cut-away view of an embodiment of a deactivatable locking assembly in a second configuration.

DETAILED DESCRIPTION OF THE EMBODIMENTS

In the drawings and description that follow, like parts are typically marked throughout the specification and drawings with the same reference numerals, respectively. In addition, similar reference numerals may refer to similar components in different embodiments disclosed herein. The drawing figures are not necessarily to scale. Certain features of the invention may be shown exaggerated in scale or in somewhat schematic form and some details of conventional elements may not be shown in the interest of clarity and conciseness. The present disclosure is susceptible to embodiments of different forms. Specific embodiments are described in detail and are shown in the drawings, with the understanding that the present disclosure is not intended to limit the invention to the embodiments illustrated and described herein. It is to be fully recognized that the different teachings of the embodiments discussed herein may be employed separately or in any suitable combination to produce desired results.

Unless otherwise specified, use of the terms "connect," "engage," "couple," "attach," or any other like term describing an interaction between elements is not meant to limit the interaction to direct interaction between the elements and may also include indirect interaction between the elements described.

Unless otherwise specified, use of the terms "up," "upper," "upward," "up-hole," "upstream," or other like terms shall be construed as generally from the formation toward the surface or toward the surface of a body of water; likewise, use of "down," "lower," "downward," "down-hole," "downstream," or other like terms shall be construed as generally into the formation away from the surface or away from the surface of a body of water, regardless of the wellbore orientation. Use of any one or more of the foregoing terms shall not be construed as denoting positions along a perfectly vertical axis.

Unless otherwise specified, use of the term "subterranean formation" shall be construed as encompassing both areas below exposed earth and areas below earth covered by water such as ocean or fresh water.

Disclosed herein are embodiments of a pressure testing valve (PTV) and method of using the same. Particularly, disclosed herein are one or more embodiments of a PTV incorporated within a tubular, for example a casing string or liner, comprising one or more wellbore servicing tools positioned within a wellbore penetrating subterranean formation.

Where a casing string has been placed within a wellbore and, for example, prior to the commencement of stimulation (e.g., fracturing and/or perforating) operations, it may be desirable to pressure test the casing string or liner and thereby verify its integrity and functionality. In the embodiments disclosed herein, a PTV enables the casing string to be pressure tested and subsequently allow a route of fluid communication from a flowbore of the casing string to the wellbore without the use of excessive pressure threshold levels.

Referring to FIG. **1**, an embodiment of an operating environment in which such a PTV may be employed is illustrated. It is noted that although some of the figures may exemplify horizontal or vertical wellbores, the principles of the methods, apparatuses, and systems disclosed herein may be similarly applicable to horizontal wellbore configurations, conventional vertical wellbore configurations, and combinations thereof. Therefore, the horizontal or vertical nature of any figure is not to be construed as limiting the wellbore to any particular configuration.

Referring to FIG. **1**, the operating environment comprises a drilling or servicing rig **106** that is positioned on the earth's surface **104** and extends over and around a wellbore **114** that penetrates a subterranean formation **102** for the purpose of recovering hydrocarbons. The wellbore **114** may be drilled into the subterranean formation **102** by any suitable drilling technique. In an embodiment, the drilling or servicing rig **106** comprises a derrick **108** with a rig floor **110** through which a casing string **150** generally defining an axial flowbore **115** may be positioned within the wellbore **114**. The drilling or servicing rig **106** may be conventional and may comprise a motor driven winch and other associated equipment for lowering the casing string **150** into the wellbore **114** and, for example, so as to position the PTV **100** and/or other wellbore servicing equipment at the desired depth.

In an embodiment the wellbore **114** may extend substantially vertically away from the earth's surface **104** over a vertical wellbore portion, or may deviate at any angle from the earth's surface **104** over a deviated or horizontal wellbore portion. In alternative operating environments, portions or substantially all of the wellbore **114** may be vertical, deviated, horizontal, and/or curved.

In an embodiment, a portion of the casing string **150** may be secured into position against the formation **102** in a conventional manner using cement **116**. In alternative embodiment, the wellbore **114** may be partially cased and cemented thereby resulting in a portion of the wellbore **114** being uncemented. In an embodiment, incorporated within the casing string **150** is a PTV **100** or some part thereof. The PTV **100** may be delivered to a predetermined depth within the wellbore. In an alternative embodiment, the PTV **100** or some part thereof may be comprised along and/or integral with a liner.

It is noted that although the PTV is disclosed as being incorporated within a casing string in one or more embodiments, the specification should not be construed as so-limiting. A wellbore servicing tool may similarly be incorporated within other suitable tubulars such as a work string, liner, production string, a length of tubing, or the like.

Referring to FIG. **1**, the casing string **150** and/or PTV **100** may additionally or alternatively be secured within the wellbore **114** using one or more packers **170**. The packer **170** may generally comprise a device or apparatus which is configurable to seal or isolate two or more depths in a wellbore from each other by providing a barrier concentrically about a casing string and therebetween. Non-limiting examples of a packer suitably employed as packer **170** include a mechanical packer or a swellable packer (for example, SwellPackers™, commercially available from Halliburton Energy Services).

While the operating environment depicted in FIG. **1** refers to a stationary drilling or servicing rig **106** for lowering and setting the casing string **150** within a land-based wellbore **114**, one of ordinary skill in the art will readily appreciate that mobile workover rigs, wellbore servicing units (e.g., coiled tubing units), and the like may be used to lower the casing string **150** into the wellbore **114**. It should be understood that a PTV may be employed within other operational environments, such as within an offshore wellbore operational environment.

In an embodiment, the PTV **100** is selectively configurable to either allow or disallow a route of fluid communication from a flowbore **124** thereof and/or the casing flowbore **115** to the formation **102** and/or into the wellbore **114**. Referring to FIGS. **4**A-**4**C, in an embodiment, the PTV **100** may generally comprise of a housing **120**, a sliding sleeve **126**, and one or more ports **122**. In an embodiment, the PTV **100** may be configured to be transitional from a first configuration to a second configuration and from the second configuration to a third configuration.

In an embodiment as depicted in FIG. **4**A, the PTV **100** is illustrated in the first configuration. In the first configuration, the PTV **100** is configured to disallow fluid communication via the one or more ports **122** of the PTV **100**. Additionally, in an embodiment, when the PTV **100** is in the first configuration, the sliding sleeve **126** is located (e.g., immobilized) in a first position within the PTV **100**, as will be disclosed herein.

In an embodiment as depicted in FIG. **4**B, the PTV **100** is illustrated in the second configuration. In the second configuration, the PTV **100** is configured to disallow fluid communication via the one or more ports **122** of the PTV **100**. In an embodiment as will be disclosed herein, the PTV **100** may be configured to transition from the first configuration to the second configuration upon the application of a pressure to the PTV **100** of at least a first or upper pressure threshold. Additionally, in an embodiment when the PTV **100** is in the second configuration, the sliding sleeve **126** is in a second position and is no longer immobilized within the PTV **100**, as will be disclosed herein.

In an embodiment as depicted in FIG. **4**C, the PTV **100** is illustrated in the third configuration. In the third configuration, the PTV **100** is configured to allow fluid communication via the one or more ports **122** of the PTV **100**. In an embodiment as will be disclosed herein, the PTV may be configured to transition from the second configuration the third configuration upon allowing the pressure applied to the PTV **100** to subside to not more than a second or lower pressure threshold. Additionally, in an embodiment when the PTV is in the third configuration, the sliding sleeve **126** is located (e.g., locked) into a third position within the PTV **100**.

FIG. **2** and FIG. **3**, together, illustrate an embodiment of the PTV **100**. In an embodiment the PTV **100** comprises a housing **120**. In the embodiment of FIG. **2** and FIG. **3**, the housing **120** of the PTV **100** is a generally cylindrical or tubular-like structure. The housing **120** may comprise a unitary structure; alternatively, the housing **120** may be made up of two or more operably connected components (e.g., an upper component, and a lower component). Alternatively, a housing of a PTV **100** may comprise any suitable structure; such suitable structures will be appreciated by those of skill in the art with the aid of this disclosure.

In an embodiment the PTV **100** may be configured for incorporation into the casing string **150**, for example, as illustrated by the embodiment of FIG. **1**, or alternatively, into any suitable string (e.g., a liner or other tubular). In such an embodiment, the housing **120** may comprise a suitable connection to the casing string **150** (e.g., to a casing string member, such as a casing joint). For example, the housing may comprise internally or externally threaded surfaces. Additional or alternative, suitable connections to a casing string will be known to those of skill in the art.

In the embodiment of FIG. **2** and FIG. **3**, the housing **120** generally defines an axial flowbore **124**. Referring to FIG. **1**, the PTV **100** is incorporated within the casing string **150** such that the axial flowbore **124** of the PTV **100** is in fluid communication with the axial flowbore **115** of the casing string **150**. For example, a fluid may be communicated between the axial flowbore **115** of the casing string **150** and the axial flowbore **124** of the PTV **100**.

In the embodiment of FIG. **2**, the housing **120** comprises one or more ports **122**. In this embodiment, the ports **122** extend radially outward from and/or inward towards the axial flowbore **124**. As such, these ports **122** may provide a route of fluid communication from the axial flowbore **124** to an exterior of the housing **120** when the PTV **100** is so-configured. For example, the PTV **100** may be configured such that the ports **122** provide a route of fluid communication between the axial flowbore **124** and the wellbore **114** and/or subterranean formation **102** when the ports **122** are unblocked (e.g., by the sliding sleeve **126**, as will be disclosed herein). Alternatively, the PTV **100** may be configured such that no fluid will be communicated via the ports **122** between the axial flowbore **124** and the wellbore **114** and/or the subterranean formation **102** when the ports **122** are blocked (e.g., by the sliding sleeve **126**, as will be disclosed herein).

In the embodiment of FIG. **2** and FIG. **3**, the housing **120** comprises a recess **138**. In the embodiment of FIG. **2** and FIG. **3**, the recess **138** is generally defined by a first bore surface **139***a*, a second bore surface **139***b*, a third bore surface **139***c*, and a fourth bore surface **139***d*. In this embodiment, the first bore surface **139***a* generally comprises a cylindrical surface spanning between an upper shoulder **138***a* and a first medial shoulder **138***e*, the second bore surface **139***b* generally comprises a cylindrical surface spanning between the first medial shoulder **138***e* and a second medial shoulder **138***c*, the third bore surface **139***c* generally comprises a cylindrical surface spanning between the second medial shoulder **138***c* and a third medial shoulder **138***d*, and the fourth bore surface **139***d* generally comprises a cylindrical surface spanning between the third medial shoulder **138***d* and a lower shoulder **138***b*.

In an embodiment, the first bore surface **139***a* may be characterized as having a diameter less than the diameter of the second bore surface **139***b*. Also, in an embodiment the third bore surface **139***c* may be characterized as having a diameter less than either the diameter of the first bore surface **139***a* or the diameter of the second bore surface **139***b*. Also, in an embodiment, the fourth bore surface **139***d* may be characterized as having a diameter greater than the diameter of the third bore surface **139***c*.

Referring to FIG. **2** and FIG. **3**, the sliding sleeve **126** generally comprises a cylindrical or tubular structure comprising an axial flowbore extending there-through. In the embodiment of FIG. **2** and FIG. **3**, the sliding sleeve **126** generally comprises a first sleeve segment **126***a*, a second sleeve segment **126***b*, and a third sleeve segment **126***c*. In such an embodiment, the first sleeve segment **126***a*, the second sleeve segment **126***b*, and the third sleeve segment **126***c* are coupled together by any suitable methods as would be known by those of skill in the art (e.g., by a threaded connection). Alternatively, the sliding sleeve **126** may comprise a unitary structure (e.g., a single solid piece).

In an embodiment, the sliding sleeve may comprise one or more of shoulders or the like, generally defining one or more outer cylindrical surfaces of various diameters. Referring to FIG. **2** and FIG. **3**, the sliding sleeve **126** comprises an upper surface **126***d*, a first medial shoulder **126***p*, a first outer cylindrical bore face **126***e* extending between the upper surface **126***d* and the first medial shoulder **126***p*, a second medial shoulder **126***f*, and a second outer cylindrical bore surface **126***m*. In an embodiment, the first outer cylindrical bore surface **126***e* may be characterized as having a diameter less than the diameter of the second outer cylindrical bore surface **126***m*. Further, the sliding sleeve **126** may comprise a third medial shoulder **126***g* and a third outer cylindrical bore surface **126***q* extending between the a second medial shoulder **126***f* and the third medial shoulder **126***g*. In an embodiment, the third outer cylindrical bore surface may be characterized as having a diameter less than the diameter of either of the first or the second outer bore surfaces, **126***e* and **126***m*. Further still, the sliding sleeve **126** may comprise a fourth medial shoulder **126***k* and a fourth outer cylindrical bore surface **126***h* extending between the third medial shoulder **126***g* and the fourth medial shoulder **126***k*. In an embodiment, the fourth outer cylindrical surface **126***h* may be characterized as having a diameter greater than the diameter of the third outer cylindrical surface **126***q*. Still further, the sliding sleeve **126** may comprise a lower surface **126***j* and a fifth outer cylindrical surface **126***i* extending between the fourth medial shoulder **126***k* and the lower surface **126***j*. In an embodiment, the fifth outer cylindrical surface **126***i* may be characterized as having a diameter less than the diameter of the fourth outer cylindrical surface **126***h*.

In an embodiment, the sliding sleeve **126** may be slidably and concentrically positioned within the housing. For example, in the embodiment of FIGS. **2** and **3**, at least a portion of the first cylindrical bore face **126***e* of the sliding sleeve **126** may be slidably fitted against at least a portion of the first bore surface **139***a* of the recess **138**. Further, at least a portion of the second outer cylindrical bore face **126***m* of the sliding sleeve **126** may be slidably fitted against at least a portion of the second bore surface **139***b* of the recess **138**. Further still, at least a portion of the third outer cylindrical bore face **126***q* of the sliding sleeve **126** may be slidably fitted against at least a portion of the third bore surface **139***c* of the recess **138**. Further still, at least a portion of the fourth outer bore face **126***h* of the sliding sleeve **126** may be slidably fitted against at least a portion of the fourth bore surface **139***d* of the sliding sleeve **138**. Further still, at least a portion of the fifth outer cylindrical bore surface **126***i* may be slidably fitted against at least a portion of a fifth bore surface **139***e* defining the axial flowbore **124**.

In an embodiment, one or more of the interfaces between the sliding sleeve **126** and the recess **138** may be fluid-tight and/or substantially fluid-tight. For example, in an embodiment, the recess **138** and/or the sliding sleeve **126** may comprise one or more suitable seals at such an interface, for example, for the purpose of prohibiting or restricting fluid movement via such an interface. Suitable seals include but are not limited to a T-seal, an O-ring, a gasket, or combinations thereof. In the embodiment of FIGS. **2** and **3**, the PTV **100** comprises a fluid seal **136***a* (e.g., one or more O-rings or the like) at the interface between the first cylindrical bore face **126***e* of the sliding sleeve **126** and the first bore surface **139***a* of the recess **138** and a fluid seal **136***b* at and/or proximate to the interface between the second outer cylindrical bore face **126***m* of the sliding sleeve **126** and the second bore surface **139***b* of the recess **138**.

In an embodiment, the sliding sleeve **126** may be movable, with respect to the housing **120**, from a first position to a second position and from the second to a third position with respect to the housing **120**.

In an embodiment, the sliding sleeve **126** may be positioned so as to allow or disallow fluid communication via the one or more ports **122** between the axial flowbore **124** of the housing **120** and the exterior of the housing **120**, dependent upon the position of the sliding sleeve **126** relative to the housing **120**. Referring to FIG. **4**A, the sliding sleeve **126** is illustrated in the first position. In the first position, the sliding sleeve **126** blocks the ports **122** of the housing **120** and, thereby, restricts fluid communication via the ports **122**. As noted above, when the sliding sleeve **126** is in the first position, the PTV **100** may be in the first configuration. Referring to FIG. **4**B, the sliding sleeve **126** is illustrated in the second position. In the second position, the sliding sleeve **126** blocks the ports **122** of the housing **120** and, thereby, restricts fluid communication via the ports **122**. Alternatively, referring to FIG. **4**C, the sliding sleeve **126** is illustrated in the third position. In the third position, the sliding sleeve **126** does not block or obstruct the ports **122** of the housing **120** and, thereby allows fluid communication via the ports **122**.

In an embodiment, the sliding sleeve **126** may be configured to be selectively transitioned from the first position to the second position and/or from the second position to the third position.

For example, in an embodiment the sliding sleeve **126** may be configured to transition from the first position to the second position upon the application of a hydraulic pressure of at least a first threshold to the axial flowbore **124**. In such an embodiment, the sliding sleeve **126** may comprise a differential in the surface area of the upward-facing surfaces which are fluidicly exposed to the axial flowbore **124** and the surface area of the downward-facing surfaces which are fluidicly exposed to the axial flowbore **124**. For example, in the embodiment of FIGS. **2** and **3**, the surface area of the surfaces of the sliding sleeve **126** which will apply a force (e.g., a hydraulic force) in the direction toward the second position (e.g., an upward force) may be greater than surface area of the surfaces of the sliding sleeve **126** which will apply a force (e.g., a hydraulic force) in the direction away from the second position. For example, in the embodiment of FIGS. **2** and **3** and not intending to be bound by theory, because the interface between the first cylindrical bore face **126***e* of the sliding sleeve **126** and the first bore surface **139***a* of the recess **138** and the interface between the second outer cylindrical bore face **126***m* of the sliding sleeve **126** and the second bore surface **139***b* of the recess **138**, as disclosed above, are fluidicly sealed (e.g., by fluid seals **136***a* and **136***b*), there is a resulting chamber **142** which is unexposed to hydraulic fluid pressures applied to the axial flowbore, thereby resulting in such a differential in the force applied to the sliding sleeve in the direction toward the second position (e.g., an upward force) and the force applied to the sliding sleeve in the direction away from the second position (e.g., a downward force). For example, the first medial shoulder **126***p* of the sliding sleeve **126** (e.g., which is within the chamber **142**) may be unexposed to the axial flowbore **124** while all other faces capable of applying a force are exposed. In an additional or alternative embodiment, a PTV like PTV **100** may further comprise one or more additional chambers (e.g., similar to chamber **142**) providing such a differential in the force applied to the sliding sleeve in the direction toward the second position (e.g., an upward force) and the force applied to the sliding sleeve in the direction away from the second position (e.g., a downward force).

Also, in an embodiment the sliding sleeve **126** may be configured to be transitioned from the second position to the third position via the operation of a biasing member. For example, in the embodiment of FIGS. **2** and **3**, the PTV **100** comprises a biasing member **128** (e.g., a biasing spring) configured to apply a biasing force to the sliding sleeve **126** in the direction of the third position. Examples of a suitable biasing member include, but are not limited to, a spring, a pneumatic device, a compressed fluid device, or combinations thereof.

Additionally or alternatively, in an embodiment, the sliding sleeve **126** may be configured to be transitioned from the second position to the third position via the operation of a floating piston assembly (FPA). Referring to FIG. **5**, an embodiment of a PTV **101** (e.g., being otherwise similar to PTV **100**) comprising a FPA **600** is illustrated. In an embodiment, the FPA **600** may be generally configured such that, when unactivated (e.g., prior to activation, as will be disclosed herein), the FPA **600** will not apply a force (alternatively, will apply only an insubstantial force) to the sliding sleeve **126** in either the direction of the second position (e.g., an upward force) or in the direction of the third position (e.g., a downward force). Also, the FPA **600** may be generally configured such that, when activated (e.g., following activation, as will be disclosed herein), the FPA **600** will apply a force to the sliding sleeve **126** in the direction of the third position (e.g., a downward force).

Referring to FIGS. **6**A and **6**B, the FPA **600** is illustrated in the activated configuration. In the embodiment of FIGS. **5**, **6**A, and **6**B, the FPA **600** generally comprises a floating piston **610**. In an embodiment, the floating piston **610** generally comprises a cylindrical, tubular, or collar-like structure. For example, in the embodiment of FIGS. **5**, **6**A, and **6**B, the floating piston **610** generally comprises an upper orthogonal surface **612**, a lower orthogonal surface **614**, an inner cylindrical surface **616**, and an outer cylindrical surface **618**.

In an embodiment, the floating piston **610** may be slidably disposed between the sliding sleeve **126** and the housing **120**. For example, in the embodiment of FIGS. **6**A and **6**B, the floating piston **610** is disposed between the sliding sleeve **126** and the housing **120** such that the inner cylindrical surface **616** of the floating piston **610** is slidably disposed against a sixth outer cylindrical bore surface **126***r* (as will be disclosed herein) and the outer cylindrical surface **618** of the floating piston **610** is slidably disposed against the second bore surface **139***b* of the housing **120**.

Additionally, in an embodiment the interface between the housing **120** and the floating piston **610** and/or the interface between the sliding sleeve **126** and the floating piston **610** may be fluid-tight and/or substantially fluid-tight. For example, in an embodiment the floating piston (alternatively, the housing **120** and/or sliding sleeve **126**) may comprise one of more suitable seals at such interfaces. Suitable seals include but are not limited to a T-seal, an O-ring, a gasket, or combinations thereof. For example, in the embodiment of FIGS. **6**A and **6**B, the floating piston **610** comprises a suitable seal **615***a* at the interface between the inner cylindrical surface **616** of the floating piston **610** and the sixth outer cylindrical bore surface **126***r* and another suitable seal **615***b* at the interface between the outer cylindrical surface **618** of the floating piston **610** and the second bore surface **139***b* of the housing **120**.

Also, in the embodiment where the PTV **101** comprises an FPA (such as FPA **600**), the sliding sleeve **126** may be configured so as to engage the floating piston **610**, for example, so as to impede downward movement of the floating piston **610** with respect to the sliding sleeve **126**, as will be disclosed herein. For example, in the embodiment of FIGS. **6**A and **6**B the sliding sleeve **126** comprises an upwardly-facing shoulder **126***s*, for example, thereby differentiating the third outer cylindrical surface **126***q* and the sixth outer cylindrical surface **126***r*. In additional or alternative embodiments, the sliding sleeve **126** may comprise one or more lugs, pins, teeth, ratchets, or the like, similarly configured to engage the floating piston **610** and restrict movement thereof.

In addition, in the embodiment where the PTV **101** comprises an FPA (such as FPA **600**), the sliding sleeve **126** may be configured to control fluidic access to one or more surfaces of the floating piston **610**. For example, in the embodiment of the FIGS. **6**A and **6**B, the sliding sleeve **126** further comprises a check-valve **620** (e.g., a uni-directional valve or one-way valve) generally configured to control fluidic access to the upper orthogonal surface **612** of the floating piston **610**. In an embodiment, the check-valve **620** may comprise any suitable type and/or configuration of a check-valve, for example, swing check valve, a tilting disc check valve, a ball check valve, or the like. Suitable examples of the check-valve **620** are commercially available as the Lee Chek line of check valves from. The Lee Company of Westbrook, Conn. In an embodiment, for example, in the embodiment of FIGS. **6**A and **6**B, the check-valve **620** may be generally configured to allow fluid to be communicated from the axial flowbore **124** through the sliding sleeve **126** to the upper orthogonal surface **612** of the floating piston **610** and to not allow fluid to be communicated from the area proximate to the upper orthogonal surface **612** to the axial flowbore **124**.

In an embodiment, the FPA **600** may be configured to be activated (e.g., so as to apply a downward force to the sliding sleeve **126**) upon the pressurization and depressurization (e.g., a pressurization, followed by a depressurization) of the axial flowbore **124**. For example, in the embodiment of FIGS. **6**A and **6**B, upon the application of pressure (e.g., a pressure of at least the upper threshold, as disclosed herein), fluid pressure may be applied to the upper orthogonal surface **612** and the lower orthogonal surface **614** of the floating piston **610**. Particularly, upon pressurization of the axial flowbore **124**, the pressure applied to the upper orthogonal surface **612** of the floating piston **610** may reach about the upper threshold (e.g., fluid and/or pressure may be communicated to the upper orthogonal surface **612** via the check valve **620**). Also, upon pressurization of the axial flowbore **124**, the pressure applied to the lower orthogonal surface **614** of the floating piston **610** may also reach the upper threshold (e.g., fluid and/or pressure may be communicated to the lower orthogonal surface **614** via the interface between the third outer cylindrical surface **126***q* and the third bore surface **139***c*, which may not be fluid-tight). For example, upon pressurization, the pressure applied to the upper orthogonal surface **612** and the lower orthogonal surface **614** may be substantially equal.

Following pressurization of the axial flowbore **124**, subsequently allowing the pressure applied to the axial flowbore **124** to dissipate may result in a differential in the pressure (e.g., and therefore, the force) applied to the upper orthogonal surface **612** and the lower orthogonal surface **614** of the floating piston **610**. Particularly, upon depressurization of the axial flowbore **124**, the pressure applied to the upper orthogonal surface **612** of the floating piston **610** may remain at about the upper threshold (e.g., the fluid and/or pressure applied to the upper orthogonal surface **612** may be retained by the check valve **620**). Also, upon depressurization of the axial flowbore **124**, the pressure applied to the lower orthogonal surface **614** of the floating piston **610** may decrease (e.g., the fluid and/or pressure applied to the lower orthogonal surface **614** may decrease to about the same pressure as the axial flowbore **124**, for example, via the interface between the third outer cylindrical surface **126***q* and the third bore surface **139***c*, which may not be fluid-tight). In such an embodiment, a differential in the pressure applied to the upper orthogonal surface **612** and the lower orthogonal surface **614** of the floating piston **610** may result upon the depressurization of the axial flowbore **124** and, therefore, result in a generally downward force applied to the floating piston **610** (and, thereby, to the sliding sleeve **126**, via the upwardly-facing shoulder **126***s*).

In an embodiment, the sliding sleeve **126** may be retained in the first position, the second position, the third position, or combinations thereof by a suitable retaining mechanism.

For example, in the embodiment of FIG. **4**A, the sliding sleeve **126** may be held in the first position by one or more shear pins **134**. Such shear pins **134** may extend between the housing **120** and the sliding sleeve **126**. The shear pin **134** may be inserted or positioned within a suitable borehole in the housing **120** and the borehole **134***a* in the sliding sleeve **126**. As will be appreciated by one of skill in the art, the shear pin **134** may be sized to shear or break upon the application of a desired magnitude of force (e.g., force resulting from the application of a hydraulic fluid pressure, such as a pressure test) to the sliding sleeve **126**, as will be disclosed herein. In an alternative embodiment, the sliding sleeve **126** may be held in the first position by any suitable frangible member, such as a shear ring or the like.

Additionally or alternatively, in an embodiment, the sliding sleeve **126** may be retained from moving from the first position in the direction of the third position by a deactivatable locking assembly (DLA). For example, in the embodiment of FIG. **5**, the PTV **101** comprises a DLA **700**. In an embodiment, the DLA **700** is generally configured such that, when activated, the DLA **700** does not allow the sliding sleeve **126** to move from the first position in the direction of the third position but does allow the sliding sleeve **126** to move from the first position in the direction of the second position. Also, the DLA **700** may be generally configured such that, when deactivated, the DLA **700** allows the sliding sleeve **126** to move from the first and/or second position in the direction of the third position.

Referring to FIGS. **7**A and **7**B, an embodiment of the DLA **700** is illustrated in the activated and deactivated configurations, respectively. In the embodiment of FIGS. **5**, **7**A, and **7**B, the DLA **700** generally comprises a locking member **710**, an outer profile **720** (e.g., disposed on an outer, cylindrical surface of the sliding sleeve **126**), and an inner profile **730** (e.g., disposed on an inner, cylindrical surface of the housing **120**).

In an embodiment, the locking member **710** comprises a ring, for example, a snap-ring, a biased C-ring, or the like. For example, in the embodiment disclosed herein with respect to

FIGS. **5**, **7**A, and **7**B, the locking member **710** comprises an outwardly-biased ring. For example, such an outwardly-biased ring may be generally configured so as to expand radially outward to an expanded conformation when not retained in a radially contracted conformation. In an alternative embodiment (for example, in an embodiment where the outer and inner profiles are reversed, with respect to the configurations disclosed with respect to FIGS. **7**A and **7**B), a locking member may be inwardly biased. In the embodiment of FIGS. **7**A and **7**B, the locking member **710** generally comprises an upper bevel and/or shoulder **712**, a lower shoulder **714**, an inner surface **716**, and an outer surface **718**.

In an embodiment, the outer profile **720** may be disposed within an outer surface of the sliding sleeve **126**. For example, in the embodiment of FIGS. **7**A and **7**B, the outer profile is disposed in the third outer cylindrical bore surface **126***q*, as disclosed herein. In alternative embodiments, an outer profile like outer profile **720** may be similarly disposed within any suitable outer surface of the sliding sleeve **126**, for example, at any suitable interface between the sliding sleeve **126** and the housing **120**. In the embodiment of FIGS. **7**A and **7**B, the outer profile **720** generally comprises an upper bevel **722**, and a lower shoulder **724**. Additionally, for example, in the embodiment of FIGS. **7**A and **7**B, the outer profile also comprises an outer recessed surface **726** extending between the upper bevel **722** and the lower shoulder **724**.

In an embodiment, the inner profile **730** may be disposed within an inner surface of the housing **120**. For example, in the embodiment of FIGS. **7**A and **7**B, the inner profile is disposed within the third bore surface **139***c* of the housing **120**, as disclosed herein. In alternative embodiments, an inner profile like inner profile **730** may be similarly disposed within any suitable inner surface of the housing, for example, at any suitable interface between the sliding sleeve **126** and the housing **120**. In the embodiment of FIGS. **7**A and **7**B, the inner profile **730** generally comprises a an upper shoulder **731**, an intermediate shoulder **733**, a lower shoulder **735**, a first inner recessed bore surface **732** extending between the upper shoulder **731** and the intermediate shoulder **733**, and a second inner recessed bore surface **734** extending between the intermediate shoulder **733** and the lower shoulder **735**. In the embodiment of FIGS. **7**A and **7**B, and as will be disclosed in greater detail herein, the first inner recessed bore surface **732** may be characterized as having a diameter greater than the diameter of the second inner recessed bore surface **734**, for example, generally providing a "stair-step" like profile.

In an embodiment, when the DLA **700** is activated (e.g., as illustrated in FIG. **7**A), for example, while the sliding sleeve **126** is in the first position, the lower shoulder **714** of the locking member **710** engages (e.g., at least partially abuts) the lower shoulder **735** of the inner profile **730** and the upper bevel/shoulder **712** engages the upper bevel **722** of the outer profile **720**. In such an embodiment, the locking member **710** is retained in the radially-inward conformation by the second inner recessed bore surface **734** (e.g., against which the outer surface **718** of the locking member **710** rests). As such, in the activated configuration, the DLA **700** may be effective to retain the sliding sleeve **126** from movement from first position in the direction of the second position, for example, via the interaction, as disclosed herein, between the locking member **710** and the outer and inner profiles, **720** and **730**, respectively. Also, when the DLA **700** is activated, the sliding sleeve **126** may be effective to hold the locking member **710** in the activated configuration; for example, the sliding sleeve **126** (e.g., the upper bevel **722** of the outer profile **720**), which may be downwardly biased (e.g., by the biasing member **128**, as disclosed herein), may exert a force effective to hold the locking member **710** in abutment with the inner profile (e.g., with the second inner recessed bore surface **734** and the lower shoulder **735**).

Also, in an embodiment, when the DLA **700** is deactivated (e.g., as illustrated in FIG. **7**B), for example, by movement of the sliding sleeve **126** from the first position toward the second position as will be disclosed herein, the locking member **710** is longitudinally aligned with the first inner recessed bore surface **732**, for example, such that the locking member **710** is not retained in the radially-inward conformation (e.g., by the second inner recessed bore surface **734**) and, as such, the locking member **710** is allowed to expand to the radially-outward conformation, for example, such that the outer surface **718** of the locking member **710** contacts the first inner bore surface **732** of the inner profile **730**. In the radially-outward conformation, the locking member **710** does not engage the sliding sleeve **126** (e.g., does not engage the outer profile **720** of the sliding sleeve **126**). As such, when deactivated, the DLA **700** will allow the sliding sleeve **126** to move from the first and/or second position in the direction of the third position, for example, in that the locking member **710** does not simultaneously interact with (e.g., engage) both the outer profile **720** and the inner profile **730**.

In an embodiment, the DLA **700** may be configured to be deactivated upon movement of the sliding sleeve **126** from the first position to the second position. For example, as disclosed herein, the DLA **700** generally does not impede movement of the sliding sleeve **126** from the first position in the direction of the second position. In an embodiment, upon movement of the sliding sleeve **126** from the first position in the direction of the second position (e.g., via the application of a fluid pressure to the differential in the upward-facing and downward-facing fluidicly exposed surfaces of the sliding sleeve **126**, as disclosed herein), the lower shoulder **724** (e.g., of the outer profile **720** of the sliding sleeve **126**) may engage the lower shoulder **714** of the locking member **710** and apply a generally longitudinally upward force to the locking member **710** so as to cause the locking member **710** to become longitudinally aligned with the first inner recessed bore surface **732**. For example, upon becoming longitudinally aligned with the first inner recessed bore, the locking member **710** is not retained in the radially-inward conformation and is allowed to expand to the radially-outward conformation, for example, thereby deactivating the locking member **710**.

Also, in the embodiment of FIG. **4**C, the sliding sleeve **126** may be retained in the third position by a locking member **130** (e.g., a snap-ring, a C-ring, a biased pin, ratchet teeth, or combinations thereof). In such an embodiment, the snap-ring (or the like) may be carried in a suitable slot, groove, channel, bore, or recess in the sliding sleeve, alternatively, in the housing, and may expand into and be received by a suitable slot groove, channel, bore, or recess in the housing, or, alternatively, in the sliding sleeve. For example, in the embodiment of FIG. **4**C, the locking member may be carried within a groove or channel within the sliding sleeve **126** and may expand into a locking groove **132** within the housing **120**.

In an embodiment, a wellbore servicing method utilizing the PTV **100** and/or system comprising a PTV **100** is disclosed herein. In an embodiment, a wellbore servicing method may generally comprise the steps of positioning the casing string **150** comprising a PTV **100** within a wellbore **114** that penetrates the subterranean formation **102**, applying a fluid pressure of at least an upper threshold within the casing string **150**, and reducing the fluid pressure within the casing string **150**. In an additional embodiment, a wellbore servicing method may further comprise one or more of the steps of allowing fluid to flow out of the casing string **150**, communicating an obturating member (e.g., a ball or dart) via the casing string, actuating a wellbore servicing tool (e.g., a wellbore stimulation tool), stimulating a formation (e.g., fracturing, perforating, acidizing, or the like), and/or producing a formation fluid from the formation.

Referring to FIG. **1**, in an embodiment the wellbore servicing method comprises positioning or "running in" a casing string **150** comprising the PTV **100**, for example, within a wellbore. In an embodiment, for example, as shown in FIG. **1**, the PTV **100** may be integrated within a casing string **150**, for example, such that the PTV **100** and the casing string **150** comprise a common axial flowbore. Thus, a fluid introduced into the casing string **150** will be communicated to the PTV **100**.

In the embodiment, the PTV **100** is introduced and/or positioned within a wellbore **114** (e.g., incorporated within the casing string **150**) in a first configuration, for example, as shown in FIG. **4**A. As disclosed herein, in the first configuration, the sliding sleeve **126** is held in the first position by at least one shear pin **134**, thereby blocking fluid communication via the ports **122** of the housing **120**. Also, the biasing member (e.g., spring) **128** is at least partially compressed and applies a force (e.g., a downward force) to the lower medial face **126***g* of the sliding sleeve **126** in the direction of the third position.

In an embodiment, positioning the PTV **100** may comprise securing the casing string with respect to the formation. For example, in the embodiment of FIG. **1**, positioning the casing string **150** having the PTV **100** incorporated therein may comprise cementing (so as to provide a cement sheath **116**) the casing string **150** and/or deploying one or more packers (such as packers **170**) at a given or desirable depth within a wellbore **114**.

In an embodiment, the wellbore servicing method comprises applying a hydraulic fluid pressure within the casing string **150** by pumping a fluid into the casing via one or more typically located at the surface, such that the pressure within the casing string **150** reaches an upper threshold. In an embodiment, such an application of pressure to the casing string **150** may comprise performing a pressure test. For example, during the performance of such a pressure test, a pressure, for example, of at least an upper magnitude, may be applied to the casing string **150** for a given duration. Such a pressure test may be employed to assess the integrity of the casing string **150** and/or components incorporated therein.

In an embodiment, the application of such a hydraulic fluid pressure may be effective to transition the sliding sleeve from the first position to the second position. For example, the hydraulic fluid pressure may be applied through the axial flowbore **124**, including to the sliding sleeve **126** of the PTV **100**. As disclosed herein, the application of a fluid pressure to the PTV **100** may yield a force in the direction of the second position, for example, because of the differential between the force applied to the sliding sleeve in the direction toward the second position (e.g., an upward force) and the force applied to the sliding sleeve in the direction away from the second position (e.g., a downward force), for example, as provided by chamber **142**.

In an embodiment, the hydraulic fluid pressure may be of a magnitude sufficient to exert a force in the direction of the second position sufficient to further compress the biasing member **128** and to shear the one or more shear pins **134**, thereby causing the sliding sleeve **126** to move relative to the housing **120** in the direction of the first position, thereby transitioning the sliding sleeve **126** from the first position to the second position. In an embodiment, the sliding sleeve may continue to move in the direction of the second position until the upper shoulder face **126***d* of the sliding sleeve **126** contacts and/or abuts the upper shoulder **138***a* of the recess **138**, thereby prohibiting the sliding sleeve **126** from continuing to slide.

In an embodiment, the upper threshold pressure may be at least about 8,000 p.s.i., alternatively, at least about 10,000 p.s.i., alternatively, at least about 12,000 p.s.i., alternatively, at least about 15,000 p.s.i., alternatively, at least about 18,000 p.s.i., alternatively, at least about 20,000 p.s.i., alternatively, any suitable pressure about equal to or less than the pressure at which the casing string **150** is rated.

Additionally, in an embodiment where the PTV (such as PTV **101**, disclosed herein) comprises a DLA (such as DLA **700**, disclosed herein), the wellbore servicing method may further comprise deactivating the DLA **700**. For example, the DLA **700** may be initially provided in an activated configuration, for example, so as to inhibit movement of the sliding sleeve **126** from the first position in the direction of the third position. In such an embodiment, deactivating the DLA **700** may comprise causing the sliding sleeve **126** to move from the first position in the direction of the second position. As disclosed herein, upon movement of the sliding sleeve **126** from the first position in the direction of the second position (e.g., via the application of a fluid pressure to the differential in the upward-facing and downward-facing fluidicly exposed surfaces of the sliding sleeve **126**, as disclosed herein), the locking member **710** will be allowed to expand to the radially-outward conformation, for example, thereby deactivating the locking member **710**. In an embodiment, and not intending to be bound by theory, the presence of a DLA (such as DLA **700**) may aid in the movement of the sliding sleeve **126**. For example, because the DLA **700** only impedes movement of the sliding sleeve **126** in the direction from the first position toward the third position (but not from the first position toward the second position), the DLA **700** may allow frangible members (e.g., shears pins **134**) having a lesser failure rating to be used (relative to otherwise similar tools not having a DLA) or, alternatively, may allow such frangible members to not be used at all (e.g., to retain the sliding sleeve **126** from movement from the first position to the third position). Also, the presence of a DLA may allow a biasing member (e.g., biasing member **128**) exerting a greater force (relative to otherwise similar tools not having a DLA) to be utilized. For example, because the DLA **700** selectively impedes movement of the sliding sleeve **126** in the direction from the first position toward the third position, the force associated with the biasing member **128** may be increased without the risk that the biasing member will inadvertently overcome the shear pins **134**.

In an embodiment, the wellbore servicing method comprises allowing the application of pressure within casing string **150** and/or the PTV **100** to fall below a lower threshold. For example, upon completion of the pressure test, for example, having assessed the integrity of the casing string **150**, the pressure applied to the casing string **150** maybe allowed to subside. In an embodiment, upon allowing the pressure within the casing string to fall below the lower threshold, the force exerted by the biasing member **128** against the sliding sleeve (e.g., against the third medial face **126***g* in the direction toward the third position is greater than the force due to hydraulic fluid pressure in the direction away from the third position (e.g., the force applied by the biasing spring **128** overcomes any frictional forces and any forces due to hydraulic fluid pressure), thereby causing the sliding sleeve **126** to move in the direction of the third position, for example until the fourth medial shoulder **126***k* comes to rest against the lower shoulder **138**b of the recess **138**, thereby transitioning the sliding sleeve **126** from the second position to the third position.

In an embodiment, the lower threshold may be less than about 6,000 p.s.i., alternatively, less than about 5,000 p.s.i., alternatively, less than about 4,000 p.s.i., alternatively, less than about 3,000 p.s.i., alternatively, less than about 2,000 p.s.i., alternatively, less than about 1,000 p.s.i., alternatively, less than about 500 p.s.i., alternatively, about 0 p.s.i.

In an embodiment, the sliding sleeve slides in the direction of the third position until the locking member **130** (e.g., a snap ring, a lock ring, a ratchet teeth, or the like) of the sliding sleeve **126** engages with an adjacent the locking groove **132** (e.g., groove, a channel, a dog, a catch, or the like) within/along the fourth bore surface **139**d of the housing **120**, thereby preventing or restricting the sliding sleeve **126** from further movement (e.g., from moving out of the third position). Thus, the sliding sleeve **126** is retained in the third position in which the ports **122** of the housing **120** are no longer blocked, thereby allowing fluid communication out of the casing string **150** (e.g., to the wellbore **114**, the subterranean formation **102**, or both) via the ports **122** of the housing **120**.

In an embodiment, following the transitioning of the sliding sleeve **126** into the third position, fluid may be allowed to escape the axial flowbore **115** of the casing **150** and the axial flowbore **124** of the PTV **100** via the ports **122** of the PTV **100**. In such an embodiment, allowing fluid to escape from the casing string **150** may allow an obturating member may be introduced within the casing string **150** and communicated therethrough, for example, so as to engage with a suitable obturating member retainer (e.g., a seat) within a wellbore servicing tool incorporated within the casing string **150**, thereby allowing actuation of such a wellbore servicing tool (e.g., opening of one or more ports, sliding sleeves, windows, etc., within a fracturing and/or perforating tool) for the performance of a formation servicing operation, for example, a formation stimulation operation, such as a fracturing, perforating, acidizing, or like stimulation operation.

In an embodiment, a wellbore servicing operation may further comprise performing a formation stimulation operation, for example, via one or more wellbore servicing tools incorporated within the casing string. Further still, following the completion of such formation stimulation operations, the wellbore servicing method may further comprise producing a formation fluid (for example, a hydrocarbon, such as oil and/or gas) from the formation via the wellbore.

Additionally, in an embodiment where the PTV (such as PTV **101**, disclosed herein) comprises a FPA (such as FPA **600**, disclosed herein), the wellbore servicing method may further comprise activating the FPA **600**. For example, the FPA **600** may be initially provided in an unactivated (e.g., a not yet activated) state. In such an embodiment, activating the FPA **600** may generally comprise pressurizing the axial flowbore **124**, followed by depressurizing the axial flowbore **124**. For example, as disclosed herein, upon the application of pressure (e.g., a pressure of at least the upper threshold, as disclosed herein), followed by the allowing the pressure applied to the axial flowbore **124** to dissipate, the FPA **600** may yield a generally downward force. In such an embodiment, the downward force may be applied to the sliding sleeve **126** (e.g., via the interaction between the floating piston **610** and the upwardly-facing shoulder **126**s of the sliding sleeve **126**) such that the sliding sleeve **126** experiences an additional downward force upon the activation of the FPA **600**.

In an embodiment, and not intending to be bound by theory, the presence of a FPA (such as FPA **600**) may aid in the movement of the sliding sleeve **126**. For example, as disclosed herein the upon activation, the FPA applies an additional force to the sliding sleeve **126** to transition the sliding sleeve **126** from the second position to the third position.

In an embodiment, a PTV **100**, a system comprising a PTV **100**, and/or a wellbore servicing method employing such a system and/or a PTV **100**, as disclosed herein or in some portion thereof, may be advantageously employed in pressure testing a casing string. For example, in an embodiment, a PTV like PTV **100** enables a casing string to be safely pressurized (e.g., tested) at a desired pressure, but does not require that such test pressure be exceeded following the pressure test in order to transition open a valve. For example, because PTV **100** can be configured to transitioned from the first configuration to the second configuration, as disclosed herein, upon any suitable pressure and because the PTV **100** does not allow fluid communication until the fluid pressure has subsided, a PTV as disclosed herein may be opened without exceeding the maximum value of the pressure test.

As may be appreciated by one of skill in the art, conventional methods of providing fluid communication following a pressure testing a casing string require, following the pressure test, over-pressuring a casing string to shear one or more shear pins and thereby enable fluid communication from the axial flowbore of the casing string to the wellbore formation. As such, conventional tools, systems, and/or methods do not provide a way to ensure the opening of one or more ports without the use of pressure levels which would generally exceed the maximal pressures used during pressure testing. Therefore, the methods disclosed herein provide a means by which pressure testing of a casing string can be performed only requiring pressure levels within the standard pressure testing levels.

ADDITIONAL DISCLOSURE

The following are nonlimiting, specific embodiments in accordance with the present disclosure:

A first embodiment, which is a wellbore servicing system comprising:

a casing string; and

a pressure testing valve, the pressure testing valve incorporated within the casing string and comprising:

- a housing comprising one or more ports and an axial flowbore; and
- a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing and transitional from:
  - a first position to a second position, and from the second position to a third position;
  - wherein, when the sliding sleeve is in the first position and the second position, the sliding sleeves blocks a route of fluid communication via the one or more ports and, when the sliding sleeve is in the third position the sliding sleeve does not block the route of fluid communication via the one or more ports;
  - wherein the pressure testing valve is configured such that application of a fluid pressure of at least an upper threshold to the axial flowbore causes the sliding sleeve to transition from the first position to the second position; and
  - wherein the pressure testing valve is configured such that a reduction of the fluid pressure to not more than a lower threshold applied to the axial flowbore causes the sliding sleeve to transition from the second position to the third position; and

a floating piston assembly slidably disposed between the housing and the sliding sleeve, wherein the floating piston assembly is configured such that,

when unactivated, the floating piston assembly will not apply a force to the sliding sleeve in either the direction of the second position or in the direction of the third position, and

when activated, the floating piston assembly will apply a force to the sliding sleeve in the direction of the third position.

A second embodiment, which is the wellbore servicing system of the first embodiment, wherein the floating piston assembly comprises a floating piston slidably disposed between the sliding sleeve and the housing.

A third embodiment, which is the wellbore servicing system of the second embodiment, wherein the sliding sleeve comprises a unidirectional valve, wherein the unidirectional valve is configured to allow fluid communication from the axial flowbore to an upper orthogonal surface of the floating piston.

A fourth embodiment, which is the wellbore servicing system of the third embodiment, wherein a lower orthogonal surface of the floating piston is fluidicly exposed to the axial flowbore.

A fifth embodiment, which is the wellbore servicing system of one of the first through the fourth embodiments, wherein the floating piston assembly is configured to be activated upon the application of a fluid pressure of at least an upper threshold to the axial flowbore followed by the reduction of the fluid pressure to not more than a lower threshold applied to the axial flowbore.

A sixth embodiment, which is the wellbore servicing system of one of the first through the fifth embodiments, wherein the sliding sleeve is biased in the direction of the third position.

A seventh embodiment, which is the wellbore servicing system of the sixth embodiment, wherein the pressure testing valve comprises a spring, wherein the spring is configured to bias the sliding sleeve towards the third position.

An eighth embodiment, which is the wellbore servicing system of one of the first through the seventh embodiments, wherein the pressure testing valve comprises one or more frangible members configured to restrain the sliding sleeve in the first position.

A ninth embodiment, which is the wellbore servicing system of one of the first through the eighth embodiments, wherein the pressure testing valve comprises a locking system comprising a lock and locking groove configured to retain the sliding sleeve in the third position.

A tenth embodiment, which is the wellbore servicing system of one of the first through the ninth embodiments, where the pressure testing valve comprises a differential area chamber, wherein the differential area chamber is not fluidicly exposed to the axial flowbore.

An eleventh embodiment, which is the wellbore servicing system of the tenth embodiment, wherein the differential area comprises of one or more o-rings.

A twelfth embodiment, which is the wellbore servicing system of one of the first through the eleventh embodiments, wherein the upper threshold is at least about 15,000 p.s.i.

A thirteenth embodiment, which is the wellbore servicing system of one of the first through the twelfth embodiments, wherein the lower threshold is not more than about 5,000 p.s.i.

A fourteenth embodiment, which is a wellbore servicing method comprising:

positioning casing string having a pressure testing valve incorporated therein within a wellbore penetrating the subterranean formation, wherein the pressure testing valve comprises:

a housing comprising one or more ports and an axial flowbore;

a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing, wherein the sliding sleeve is configured to block a route of fluid communication via one or more ports when the casing string is positioned within the wellbore; and

a floating piston assembly slidably disposed between the housing and the sliding sleeve, wherein the floating piston assembly is configured so as to not apply longitudinal force to the sliding sleeve;

applying a fluid pressure of at least an upper threshold to the axial flowbore, wherein, upon application of the fluid pressure of at least the upper threshold, the sliding sleeve continues to block the route of fluid communication and the floating piston assembly continues to not apply a longitudinal force to the sliding sleeve; and

reducing the fluid pressure to not more than a lower threshold, wherein, upon reduction of the fluid pressure to not more than the lower threshold, the sliding sleeve allows fluid communication via one or more ports of the housing and the floating piston assembly applies a downward force to the sliding sleeve.

A fifteenth embodiment, which is the method of the fourteenth embodiment, wherein the floating piston assembly comprises a floating piston slidably disposed between the sliding sleeve and the housing.

A sixteenth embodiment, which is the method of the fifteenth embodiment, wherein upon application of the fluid pressure of at least the upper threshold and reduction of the fluid pressure to not more than the lower threshold, a fluid pressure applied to an upper orthogonal surface of the floating piston is greater than a fluid pressure applied to a lower orthogonal surface of the floating piston.

A seventeenth embodiment, which is a wellbore servicing tool comprising:

a housing comprising an axial flowbore; and

a sliding sleeve, wherein the sliding sleeve is slidably, longitudinally movable within the housing; and

a floating piston assembly slidably disposed between the housing and the sliding sleeve, wherein the floating piston is configured such that,

when unactivated, the floating piston assembly will not apply a force to the sliding sleeve in either a first longitudinal direction or a second longitudinal direction, and

when activated, the floating piston assembly will apply a force to the sliding sleeve in the first longitudinal direction.

An eighteenth embodiment, which is the wellbore servicing tool of the seventeenth embodiment, wherein the floating piston assembly is configured to be activated upon the application of a fluid pressure to the axial flowbore followed by the reduction of the fluid pressure applied to the axial flowbore.

A nineteenth embodiment, which is the wellbore servicing tool of one of the seventeenth through the eighteenth embodiments, wherein the floating piston assembly comprises a floating piston slidably disposed between the sliding sleeve and the housing.

A twentieth embodiment, which is the wellbore servicing tool of the nineteenth embodiment, wherein the sliding sleeve comprises a unidirectional valve, wherein the unidirectional valve is configured to allow fluid communication from the axial flowbore to a first orthogonal surface of the floating piston.

A twenty-first embodiment, which is the wellbore servicing tool of the twentieth embodiment, wherein a second orthogonal surface of the floating piston is fluidicly exposed to the axial flowbore.

A twenty-second embodiment, which is a wellbore servicing system comprising:

- a casing string; and
- a pressure testing valve, the pressure testing valve incorporated within the casing string and comprising:
  - a housing comprising one or more ports and an axial flowbore; and
  - a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing and transitional from:
    - a first position to a second position, and from the second position to a third position;
      - wherein, when the sliding sleeve is in the first position and the second position, the sliding sleeves blocks a route of fluid communication via the one or more ports and, when the sliding sleeve is in the third position the sliding sleeve does not block the route of fluid communication via the one or more ports;
      - wherein the pressure testing valve is configured such that application of a fluid pressure of at least an upper threshold to the axial flowbore causes the sliding sleeve to transition from the first position to the second position; and
      - wherein the pressure testing valve is configured such that a reduction of the fluid pressure to not more than a lower threshold applied to the axial flowbore causes the sliding sleeve to transition from the second position to the third position; and
  - a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured such that,
    - when activated, the deactivatable locking assembly will inhibit movement of the sliding sleeve in the direction of the third position, and
    - when deactivated, the deactivatable locking assembly will not inhibit movement of the sliding sleeve in the direction of the third position.

A twenty-third embodiment, which is the wellbore servicing system of the twenty-second embodiment, wherein the deactivatable locking assembly comprises:

- an outer profile, wherein the outer profile is disposed on an outer surface of the sliding sleeve;
- an inner profile, wherein the inner profile is disposed on an inner surface of the housing; and
- a locking member disposed between the sliding sleeve and the housing.

A twenty-fourth embodiment, which is the wellbore servicing system of the twenty-third embodiment,

- wherein the outer profile comprises an upward-facing, lower shoulder and an upper bevel,
- wherein the inner profile comprises a downward-facing upper shoulder, an upward-facing intermediate shoulder, an upward-facing lower shoulder, a first cylindrical surface extending between the upper shoulder and the intermediate shoulder, and a second cylindrical surface extending between the intermediate shoulder and the lower shoulder, and
- wherein the locking member comprises a outwardly biased ring.

A twenty-fifth embodiment, which is the wellbore servicing system of the twenty-fourth embodiment, wherein, when the deactivatable locking assembly is activated, the locking member engages the lower shoulder of the inner profile and the upper bevel of the outer profile.

A twenty-sixth embodiment, which is the wellbore servicing system of one of the twenty-fourth through the twenty-fifth embodiments, wherein, when the deactivatable locking assembly is deactivated, the locking member engages only one of the outer profile and the inner profile.

A twenty-seventh embodiment, which is the wellbore servicing system of one of the twenty-fourth through the twenty-sixth embodiments,

- wherein the first cylindrical surface of the inner profile is characterized as having a diameter greater than the second cylindrical surface of the inner profile
- wherein, when the locking member is aligned with the second cylindrical surface, the deactivatable locking assembly is activated, and
- wherein, when the locking member is aligned with the first cylindrical surface, the deactivatable locking assembly is deactivated.

A twenty-eighth embodiment, which is the wellbore servicing system of one of the twenty-second through the twenty-seventh embodiments, wherein the deactivatable locking assembly is configured to be deactivated upon the movement of the sliding sleeve from the first position in the direction of the second position.

A twenty-ninth embodiment, which is the wellbore servicing system of one of the twenty-second through the twenty-eighth embodiments, wherein the sliding sleeve is biased in the direction of the third position.

A thirtieth embodiment, which is the wellbore servicing system of the twenty-ninth embodiment, wherein the pressure testing valve comprises a spring, wherein the spring is configured to bias the sliding sleeve towards the third position.

A thirty-first embodiment, which is the wellbore servicing system of one of the twenty-second through the thirtieth embodiments, wherein the pressure testing valve comprises one or more frangible members configured to restrain the sliding sleeve in the first position.

A thirty-second embodiment, which is the wellbore servicing system of one of the twenty-second through the thirty-first embodiments, wherein the pressure testing valve comprises a locking system comprising a lock and locking groove configured to retain the sliding sleeve in the third position.

A thirty-third embodiment, which is the wellbore servicing system of one of the twenty-second through the thirty second embodiments, where the pressure testing valve comprises a differential area chamber, wherein the differential area chamber is not fluidicly exposed to the axial flowbore.

A thirty-fourth embodiment, which is the wellbore servicing system of the thirty-third embodiment, wherein the differential area comprises of one or more o-rings.

A thirty-fifth embodiment, which is the wellbore servicing system of one of the twenty-second through the thirty-fourth embodiments, wherein the upper threshold is at least about 15,000 p.s.i.

A thirty-sixth embodiment, which is the wellbore servicing system of one of the twenty-second through the thirty-fifth embodiments, wherein the lower threshold is not more than about 5,000 p.s.i.

A thirty-seventh embodiment, which is a wellbore servicing method comprising:

positioning casing string having a pressure testing valve incorporated therein within a wellbore penetrating the subterranean formation, wherein the pressure testing valve comprises:

a housing comprising one or more ports and an axial flowbore;

a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing in a first position in which the sliding sleeve is configured to block a route of fluid communication via one or more ports when the casing string is positioned within the wellbore; and

a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured so as to inhibit movement of the sliding sleeve in the direction of a third position;

applying a fluid pressure of at least an upper threshold to the axial flowbore, wherein, upon application of the fluid pressure of at least the upper threshold, the sliding sleeve transitions to a second position in which the sliding sleeve continues to block the route of fluid communication, and wherein, upon movement of the sliding sleeve from the first position in the direction of the second position, the deactivatable locking assembly is configured so as to not inhibit movement of the sliding sleeve in the direction of a third position; and

reducing the fluid pressure to not more than a lower threshold, wherein, upon reduction of the fluid pressure to not more than the lower threshold, the sliding sleeve transitions to a third position in which the sliding sleeve allows fluid communication via one or more ports of the housing.

A thirty-eighth embodiment, which is the method of the thirty-seventh embodiment, wherein the floating piston assembly comprises:

an outer profile, wherein the outer profile is disposed on an outer surface of the sliding sleeve;

an inner profile, wherein the inner profile is disposed on an inner surface of the housing; and

a locking member disposed between the sliding sleeve and the housing.

A thirty-ninth embodiment, which is a wellbore servicing tool comprising:

a housing comprising an axial flowbore; and

a sliding sleeve, wherein the sliding sleeve is slidably, longitudinally movable within the housing; and

a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured such that,

when activated, the deactivatable locking assembly will inhibit movement of the sliding sleeve in a first longitudinal direction and will not inhibit movement in a second longitudinal direction, wherein the first direction is generally opposite of the second direction, and

when deactivated, the deactivatable locking assembly will not inhibit movement of the sliding sleeve the first direction.

A fortieth embodiment, which is the wellbore servicing tool of the thirty-ninth embodiment, wherein the deactivatable locking assembly comprises:

an outer profile, wherein the outer profile is disposed on an outer surface of the sliding sleeve;

an inner profile, wherein the inner profile is disposed on an inner surface of the housing; and

a locking member disposed between the sliding sleeve and the housing.

A forty-first embodiment, which is the wellbore servicing tool of the fortieth embodiment, wherein the inner profile comprises a first cylindrical surface and a second cylindrical surface, wherein the first cylindrical surface of the inner profile is characterized as having a diameter greater than the second cylindrical surface of the inner profile, and wherein the locking member comprises a outwardly biased ring.

A forty-second embodiment, which is the wellbore servicing tool of the forty-first embodiment,

wherein, when the locking member is aligned with the second cylindrical surface, the deactivatable locking assembly is activated, and

wherein, when the locking member is aligned with the first cylindrical surface, the deactivatable locking assembly is deactivated.

A forty-third embodiment, which is the wellbore servicing tool of one of the forty-first through the forty-second embodiments, wherein the first cylindrical surface of the inner profile is characterized as being located in the second direction relative to the second cylindrical surface of the inner profile.

A forty-fourth embodiment, which is the wellbore servicing system of one of the thirty-ninth through the forty-third embodiments, wherein the deactivatable locking assembly is configured to be deactivated upon the movement of the sliding sleeve in the second direction.

A forty-fifth embodiment, which is the wellbore servicing system of one of the thirty-ninth through the forty-fourth embodiments, wherein the sliding sleeve is biased in the first direction.

While embodiments of the invention have been shown and described, modifications thereof can be made by one skilled in the art without departing from the spirit and teachings of the invention. The embodiments described herein are exemplary only, and are not intended to be limiting. Many variations and modifications of the invention disclosed herein are possible and are within the scope of the invention. Where numerical ranges or limitations are expressly stated, such express ranges or limitations should be understood to include iterative ranges or limitations of like magnitude falling within the expressly stated ranges or limitations (e.g., from about 1 to about 10 includes, 2, 3, 4, etc.; greater than 0.10 includes 0.11, 0.12, 0.13, etc.). For example, whenever a numerical range with a lower limit, Rl, and an upper limit, Ru, is disclosed, any number falling within the range is specifically disclosed. In particular, the following numbers within the range are specifically disclosed: $R=Rl+k*(Ru-Rl)$, wherein k is a variable ranging from 1 percent to 100 percent with a 1 percent increment, i.e., k is 1 percent, 2 percent, 3 percent, 4 percent, 5 percent, . . . 50 percent, 51 percent, 52 percent, . . . , 95 percent, 96 percent, 97 percent, 98 percent, 99 percent, or 100 percent. Moreover, any numerical range defined by two R numbers as defined in the above is also specifically disclosed. Use of the term "optionally" with respect to any element of a claim is intended to mean that the subject element is required, or alternatively, is not required. Both alternatives are intended to be within the scope of the claim. Use of broader terms such as comprises, includes, having, etc. should be understood to provide support for narrower terms such as consisting of, consisting essentially of, comprised substantially of, etc.

Accordingly, the scope of protection is not limited by the description set out above but is only limited by the claims which follow, that scope including all equivalents of the subject matter of the claims. Each and every claim is incorporated into the specification as an embodiment of the present invention. Thus, the claims are a further description and are an addition to the embodiments of the present invention. The discussion of a reference in the Detailed Description of the Embodiments is not an admission that it is prior art to the present invention, especially any reference that may have a publication date after the priority date of this application. The disclosures of all patents, patent applications, and publications cited herein are hereby incorporated by reference, to the extent that they provide exemplary, procedural or other details supplementary to those set forth herein.

What is claimed is:

1. A wellbore servicing system comprising:
a casing string; and
a pressure testing valve, the pressure testing valve incorporated within the casing string and comprising:
a housing comprising one or more ports and an axial flowbore; and
a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing and transitional from:
a first position to a second position, and from the second position to a third position;
wherein, when the sliding sleeve is in the first position and the second position, the sliding sleeve blocks a route of fluid communication via the one or more ports and, when the sliding sleeve is in the third position the sliding sleeve does not block the route of fluid communication via the one or more ports;
wherein the pressure testing valve is configured such that application of a fluid pressure of at least an upper threshold to the axial flowbore causes the sliding sleeve to transition from the first position to the second position; and
wherein the pressure testing valve is configured such that a reduction of the fluid pressure to not more than a lower threshold applied to the axial flowbore causes the sliding sleeve to transition from the second position to the third position;
a deactivatable locking assembly disposed between the housing and the sliding sleeve,
wherein when the locking assembly is activated, it will inhibit movement of the sliding sleeve in the direction of the third position, and
when the locking assembly is deactivated, it will not inhibit movement of the sliding sleeve in the direction of the third position; and
wherein the pressure testing valve comprises a locking system comprising a lock and locking groove configured to retain the sliding sleeve in the third position.

2. The wellbore servicing system of claim 1, wherein the deactivatable locking assembly comprises:
an outer profile, wherein the outer profile is disposed on an outer surface of the sliding sleeve;
an inner profile, wherein the inner profile is disposed on an inner surface of the housing; and
a locking member disposed between the sliding sleeve and the housing.

3. The wellbore servicing system of claim 2,
wherein the outer profile comprises an upward-facing, lower shoulder and an upper bevel,
wherein the inner profile comprises a downward-facing upper shoulder, an upward-facing intermediate shoulder, an upward-facing lower shoulder, a first cylindrical surface extending between the upper shoulder and the intermediate shoulder, and a second cylindrical surface extending between the intermediate shoulder and the lower shoulder, and
wherein the locking member comprises a outwardly biased ring.

4. The wellbore servicing system of claim 3, wherein, when the deactivatable locking assembly is activated, the locking member engages the lower shoulder of the inner profile and the upper bevel of the outer profile.

5. The wellbore servicing system of claim 3, wherein, when the deactivatable locking assembly is deactivated, the locking member engages only one of the outer profile and the inner profile.

6. The wellbore servicing system of claim 3,
wherein the first cylindrical surface of the inner profile is characterized as having a diameter greater than the second cylindrical surface of the inner profile
wherein, when the locking member is aligned with the second cylindrical surface, the deactivatable locking assembly is activated, and
wherein, when the locking member is aligned with the first cylindrical surface, the deactivatable locking assembly is deactivated.

7. The wellbore servicing system of claim 1, wherein the deactivatable locking assembly is configured to be deactivated upon the movement of the sliding sleeve from the first position in the direction of the second position.

8. The wellbore servicing system of claim 1, wherein the sliding sleeve is biased in the direction of the third position.

9. The wellbore servicing system of claim 8, wherein the pressure testing valve comprises a spring, wherein the spring is configured to bias the sliding sleeve towards the third position.

10. The wellbore servicing system of claim 1, wherein the pressure testing valve comprises one or more frangible members configured to restrain the sliding sleeve in the first position.

11. The well bore servicing system of claim 1, where the pressure testing valve comprises a differential area chamber, wherein the differential area chamber is not fluidicly exposed to the axial flowbore.

12. The wellbore servicing system of claim 11, wherein the differential area comprises of one or more o-rings.

13. The wellbore servicing system of claim 1, wherein the upper threshold is at least about 15,000 p.s.i.

14. The wellbore servicing system of claim 1, wherein the lower threshold is not more than about 5,000 p.s.i.

15. A wellbore servicing method comprising:
positioning a casing string having a pressure testing valve incorporated therein within a wellbore penetrating the subterranean formation, wherein the pressure testing valve comprises:
a housing comprising one or more ports and an axial flowbore;
a sliding sleeve, wherein the sliding sleeve is slidably positioned within the housing in a first position in which the sliding sleeve is configured to block a route of fluid communication via one or more ports when the casing string is positioned within the wellbore; and
a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured so as to inhibit movement of the sliding sleeve in the direction of a third position;
applying a fluid pressure of at least an upper threshold to the axial flowbore, wherein, upon application of the fluid pressure of at least the upper threshold, the sliding sleeve transitions to a second position in which the sliding sleeve continues to block the route of fluid communication, and wherein, upon movement of the sliding sleeve from the first position in the direction of the second

position, the deactivatable locking assembly is configured so as to not inhibit movement of the sliding sleeve in the direction of a third position;

reducing the fluid pressure to not more than a lower threshold, wherein, upon reduction of the fluid pressure to not more than the lower threshold, the sliding sleeve transitions to a third position in which the sliding sleeve allows fluid communication via one or more ports of the housing; and

a floating piston assembly slidably disposed between the housing and the sliding sleeve, wherein the floating piston assembly comprises:

an outer profile, wherein the outer profile is disposed on an outer surface of the sliding sleeve;

an inner profile, wherein the inner profile is disposed on an inner surface of the housing; and

a locking member disposed between the sliding sleeve and the housing.

16. A wellbore servicing tool comprising:

a housing comprising an axial flowbore; and

a sliding sleeve, wherein the sliding sleeve is slidably, longitudinally movable within the housing among a first, a second, and a third position; and

a deactivatable locking assembly disposed between the housing and the sliding sleeve, wherein the deactivatable locking assembly is configured such that,

when activated, the deactivatable locking assembly will inhibit movement of the sliding sleeve in a first longitudinal direction and will not inhibit movement in a second longitudinal direction, wherein the first direction is generally opposite of the second direction, and

when deactivated, the deactivatable locking assembly will not inhibit movement of the sliding sleeve in the first direction; wherein the deactivatable locking assembly comprises:

an outer profile, wherein the outer profile is disposed on an outer surface of the sliding sleeve;

an inner profile, wherein the inner profile is disposed on an inner surface of the housing; and

a locking member disposed between the sliding sleeve and the housing;

wherein the inner profile comprises a first cylindrical surface and a second cylindrical surface;

wherein the first cylindrical surface of the inner profile is characterized as having a diameter greater than the second cylindrical surface of the inner profile; and

wherein the locking member comprises an outwardly biased ring.

17. The wellbore servicing tool of claim **16**,

wherein, when the locking member is aligned with the second cylindrical surface, the deactivatable locking assembly is activated, and

wherein, when the locking member is aligned with the first cylindrical surface, the deactivatable locking assembly is deactivated.

18. The wellbore servicing tool of claim **16**, wherein the first cylindrical surface of the inner profile is characterized as being located in the second direction relative to the second cylindrical surface of the inner profile.

19. The wellbore servicing system of claim **16**, wherein the deactivatable locking assembly is configured to be deactivated upon the movement of the sliding sleeve in the second direction.

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